MH-53M HELICO	PTER SN:	69-5794	PAGE 15 OF 20 PAGES
DATE A	REMARKS 8	COPY	ORGANIZATION C
31 MAR 89	TCTO [H-53-581 – WAS COMPLIED WITH TCTO 1H-53-774 – WAS COMPLIED WITH TCTO 1H-53-691 – WAS COMPLIED WITH TCTO 1H-53-672 – WAS COMPLIED WITH TCTO 1H-53-808 – WAS COMPLIED WITH TCTO 1H-53-670 – WAS COMPLIED WITH TCTO 1H-53-572 – WAS COMPLIED WITH		NADEP PNCLA , FL
01 MAY 89	REFURB C/W		1 SOW NADEP PNCLA; FL
26 APR 89	TCTO 1H-53-804 – REWIRING AUXILARY FUEL FLOW LIGHTS		NADEP PNCLA, FL
12 MAY 89	AIRCRAFT RECEIVED THIS STATION FOR ASSIGNMENT @ 5876.0 A/C	CHRS.	1550 CCTW KAFB, NM
19 MAY 89	C/W ANNUAL REVIEW OF ACFT HISTORICAL FORMS		1550 CCTW KAFB, NM
12 APR 90	ACE INSP PERFORMED AT KIRTLAND AFB, AT 6400.7 A/C HRS ON 12 MEMBER L.A. KHARFENSTINE NADEP PENSACOLA.	APR 90 BY ACE TEAM	1550 CCTW KAFB, NM
05 MAR 91	ACE INSP PERFORMED AT KIRTLAND AFB, AT 6872.8 ACFT HRS ON MEMBER L.A. KHARFENSTINE NADEP PENSACOLA.	D5 MAR 91 BY ACE TEAM	1550 CCTW KAFB, NM
7 T 10 DEC 91 3	AGET DEPARTING THIS STATION FOR NADEP, PNGLAFE FOR SLEP	MOD AT UNK A/C HRS: 100 A 100	542 CTW KAFB, NM
07 FEB 92	MH53J 69-05794 RECEIVED AT NADEP PENSACOLA FOR SLEP/MOD V	VITH 7461.2 A/C HRS.	NADEP PNCLA, FL
04 AUG 92	"ARC-186 ANTENNA RELOCATION IAW WR-ALC/LUP MEMO AND DI	RAFT TCTO"	NADEP PNCLA, FL
13 JUL 92	REPLACED TRANSITION SECTION, REMOVED FROM BUNO: 68-10366 CONFIGURED PER SOW: 89 MMXSR-008-H53 PARA 3.2.2.6, A/C TIME,	,	NADEP PNCLA, FL
30 JUL 92	FITTING ASSY, PN: 9144932-10, S/TSN: P003, L/H UPPER TAIL PYLON INSTALLED IAW 50K INSTALLATION AFT FUSELAGE MOD TCTO 1H		NADEP PNCLA, FL
07 OCT 92	OTI #L209021 EMERGENCY CONTROL PANEL. S/TSN: S-38		NADEP PNCLA
20 OCT 92	EXTENDED PITCH CONTROL ROD END 3 1/2 TURNS IN R. H. ELECT C CYCLIC STICK INSTRUMENT PANEL INTERFERENCE. RIG PIN C CA		NADEP PNCLA
L]	······································	<u> </u>

DATE	remarks COPY	ORGANIZATION
09 MAY 85	ONE TIME INSP MGB TAIL IDLER GEAR LOCKING BOLT. FOR SECURITY, C/W THIS DATE	41 CAMS MCCLELLAN CA
15 MAY 84	A/C 69-05794 HH53C ARRIVED AT NARF PNCLA FOR DMISA NAVAIR76 26BFTG WITH 4618.6 A/C HRS. ACI WR/H-53-84/1 WAS COMPLETED ON 15 MAY 85.	NARF PNCLA, FL
24 MAY 85	ACFT RECEIVED THIS STATION FROM NAVAIREWORKFAC PENSACOLA, FL. ACI @ 4601.4 A/C HRS ON THIS DATE.	41 CAMS MCCLELLAN CA
14 NOV 85	C/W CLASS 1B MOD REPOS OF KY-75 FOR CREW AS OF 28 AUG 85	41 CAMS MCCLELLAN CA
30 JAN 86	OTI ALL HH53B/C ACFT ENG CANNON PLUGS/CONN C/W THIS DATE.	41 CAMS MCCLELLAN CA
09 JAN 86	OTI PROPER ROUTING OF SERVO HYD LINES C/W THIS DATE.	41 CAMS MCCLELLAN CA
05 FEB 86	23AF MSG 042100Z FEB 86, AND QA LTR. DTD 05 FEB 86, OTI ROTATING SCISSORS UPPER LINK FOR SPECIFIC PN: C/W THIS DATE.	41 CAMS MCCLELLAN CA
09 MAY 86	OTI OF POLOT/COPILOT ESCAPE WINDOWS C/W THIS DATE. OTI RESCUE HOIST SUPPORT C/W THIS DATE.	41 CAMS MCCLELLAN CA
24 APR 86	OTI ON TAIL PYLON BRACES FOR CRACKS C/W THIS DATE	41 CAMS MCCLELLAN CA
06 FEB 86	OTI HH53B/C ACFT-ENG CANNON PLUGS/CONN C/W THIS DATE.	41 CAMS MCCLELLAN CA
18 JUN 86	OTI OF CABIN HYD LINES FOR CHAFFING AND WEAR C/W THIS DATE. CLASS 1B MOC INSTL AIRCREW WPNS SECURITY BOXES C/W THIS DATE.	41 CAMS MCCLELLAN CA
29 OCT 86	ACFT 69-05794 ARRIVED THIS STATION @ 5141.1 A/C HRS.	1 SOW HFLD, FL
11 AUG 88	ACFT DEPARTED THIS STATION FOR PENSACOLA FL @ 5847.5 A/C HRS.	1 SOW HFLD, FL
03 MAR 89	OMIT FLIGHT CONTROL RIG PIN "C" DUE TO LENGTHENING ROD 2 TURNS IN R/H "E" BAY, TO BRING CONTROL STICK OFF INSTRUMENT PANEL	NADEP PNCLA, FL
31 MAR 89	A/C MH-53J ARRIVED AT NADEP PNCLA ON 11 AUG 1988 FOR J MOD CONVERSION WITH 5848.8 A/C HRS. J MOD CONVERSION WR/H-53/89-3/1 WAS COMPLETED ON 31 MAR 89	NADEP PNCLA, FL

	SIG	INIFICANT HISTORICAL DATA		PAGE 1 OF 1 PAGES
1. MISSION, DESIGN, SEI	RIES, TYPE, MODEL AND SERIES	2. MANUFACTURER	3. SERIAL NUMBER	4. ACCEPTANCE DATA
INTERMEDIA	ATE GEARBOX, 65357-07000-060	SIKORSKY	A18-235	UNKNOWN
DATE A		REMARKS B		ORGANIZATION C
14 FEB 1969	COMPLIED WITH TCTO 50-73	& 50-88 ·		SIKORSKY
06 DEC 1973	INSTALLED ON A/C CH53A-15	1686 @ 640.0 A/C HRS. IGB TSN: 1487	7.0, TSO: 0.0	NARF PNCLA, FL
11 JAN 1985	REMOVED FROM A/C CH53A-1 REASON" HI-TIME WAJ-294-80	51686 @ 2634.0 A/C HRS. IGB TSN: 3 6	481.0, TSO: 1994.0	NARF PNCLA, FL
20 FEB 1986	OVERHAULED: & NO LOAD TI	ESTED IAW NA 03-95B-102 & TI 51-1	9 & 74-88 IGB TSN: 3481.0, TSO: 0.0	NARF PNCLA, FL
06 JUN 1988	INSTALLED ON A/C CH-53D-15	57143 @ 6411.0 A/C HRS, IGB TSN: 34	81.0, TSO: 0.0	NARF PNCLA, FL
06 JUN 1988	COMPLIED ON SOAP IAW NAV	/MATINST 4731.1A. SOAP LAB LACA	ATED AT KADENA AFB	NARF PNCLA, FL
23 AUG 1989	NOAP NORMAL AT KIMHAE A	B, KOREA PRIOR TO TRANSFER		NARF PNCLA, FL
15 OCT 1991	PLACED ON NOAP W/ MONITO	DRING LABS LOCATED AT NAS LEM	MOORE, CA	NARF PNCLA, FL
20 APR 1992	REWORKED FROM NOAP			NARF PNCLA, FL
03 APR 1993	NOAP OIL SAMPLES CHECKER	O GOOD AT NADEP PNCLA LAB		NARF PNCLA, FL
28 APR 1993	NOAP INITIATED AT MCGUIR	E AFB, NJ IAW NAVMATINST 4731.1	l.A	MCGUIRE AFB, NJ
17 JUL 1993	NOAP TERMINATED AT MCGU	JIRE AFB, NJ IAW NAVMATINST 47.	31.1A	MCGUIRE AFB, NJ
2004-10-20	REMOVED FROM A/C CH-53D- REASON: UNKNOWN	157143 @ 7616.3 A/C HRS. IGB TSN:	4686.3, TSO: 1205.3	NARF PNCLA, FL
2005-05-27	RECEIVED BY AIR FORCE, AF PREVIOUS HISTORY TRANSCI	TO FORM 95 HISTORICAL ARCHIVE RIBED THIS DATE.	E INITIATED PER T.O.1H-53(M) J-6.	WR-ALC/LUJC
2005-05-27	OVERHAULED: & NO LOAD TO IGB TSN: 4686,3, TSO: 0.0	EST IAW NAVAIR 03-95B-102 & AFTI	I 2005-009 & -029	NADEP CP, NC
2005-06-05	INSTALLED ON A/C 69-05794 @	@ 11220.7 A/C HRS. IGB TSN: 4686.3,	TSO: 0.0	16 HMXS HFLD, FL

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	125.00	· · · · · · · · · · · · · · · · · · ·	160,000	·	}i	00 PS.I.	220,00	0 RS.I.	SHEA	<u> </u>	<u></u>	ISION	· · · · · · · · · · · · · · · · · · ·	EAR	-dep-
	<u> </u>	NUT	BOLT	NUT	BOLT	NUT	BOLT	NUT	BOLT	NUT		UTS NOTE 4		**********	, and a second
THREAD SIZE	ANS THRU AN20 AN173 THRU AN189 MS20073	MS21040 MS21043 MS21044 MS21045	MS20004 THRU MS20024 MS21008 NAS484 NAS1103 THRU1120 NAS1303 THRU1320 NAS6203 THRU6220	MS21042 NAS1291 SS5081 SS5086 SS5086 ESNA EB SPG 42FW	THRU 644	ESNA EB 6PS – 42FW 595081 555086 555089 FBL10015	SPS EWB22	######################################	}	AND VARION OF THE PROPERTY OF	ANTE THREE ANTE	0 :1551 ; 1576	ANS	34 50426 J 50450 7826 J354 1083 1224	de de la comercia de La comercia de la co
											MIN	MAX	MIN	MAX	· · · · · · · · · · · · · · · · · · ·
10-32 .1900-32	50	45	55	50	50	55	85	60	23	18	20	45	12	50	Andrew Andrew
1/4 .250028	110	100	125	110	- 135	120	150	135	48	43	50	100	30	50	gre des maggies
5/16 .312524	185	165	190	180	225	200	260	230	93	83	100	165	60	100	on management of
3/8 .3750-24	325	275	375	320	406	345	460	395	165	138	165	275	80	185	19
7/16 .4375-20	550	450	640	520	890	560	770	640	275	225	270	450	100	270	4)7/27/0
1/2 .5000 - 2 0	770	670	590	780	960	840	1090	950	385	335	340	570	170	340	1
9/16 .5625 - 18	1100	1000	1280	1160	1380	1250	1600	1480	560	300	500	1000	250	500	C
5/8 ,5250-18	1550	1350	1800	1570	1940	1690	2200	1930	775	675	680	1350	340	880	g
3/4 .7500-16	2700	2400	3130	2780	3380	3000	3880	3420	1350	1200	1200	2400	600	1200	4/6/94/2
7/8 .8750-14	4100	3700	4730	4270	510O	4600	5800	5250	2060	1850	1850	3700	926	1850	
1 1.000012 1.000014	5900	5360	6850	6120	7400	56QO	8450	759¢	2950	2650	2650	5300	1325	2650	
1-1/8,1,1250-12	8500	7500	9800	8700	10600	9400	12000	10750	4250	3760	2850	7500	1875	3750	(4)
1-1/4 1.250-12	12000	10000	13900	11800	15000	12500	17000	14300	8000	5000	5000	10000	2500	5010	12
NOTES: 1. UNLESS OT AND NON— THE NUT, R. 2. TORQUE VA 3. THE BOLT U USTED IN N. TO THE RIGHT	LUBRICA ATHER TI LUES FC JSED DET JORE THA INT OF TH	TED THAI HAN THE VR NUTS \ TERMINES AN ONE C HE BOLT I	SADS. TOL BOLT, SHA MITH BAKE STHE TOR COLLIMIN, IT JSED.	ERANCE LL BE TOF D ON DR' QUE REQ 'SHAUL B	ON VALI ROUED / FILM LI UIREMEI E TORQI	JES SPEC JBRICAN NT FOR T JED TO T	IFIED IN T SHALL HE NUT. HE VALL	TABLE: BE AS S THERE JE IN TH	2 IS ± RPECIF FORE E NUT	5%. W FIED IN . ALTH F COLL	MEN F JTHE OUGH JMN IN	PRACTI FD. A NUT MEDI/	CABLI MAY I	·	2 (2) (2) THE

NOTES:

- 1, UNLESS OTHERWISE SPECIFIED IN THE FD, VALUES SHOWN ARE IN INCH POUNDS AND APPLY TO LUBRICATED AND NON-LUBRICATED THREADS. TOLERANCE ON VALUES SPECIFIED IN TABLE 2 IS ±5%. WHEN PRACTICABLE, THE NUT, RATHER THAN THE BOLT, SHALL BE TORQUED.
- 2. TORQUE VALUES FOR NUTS WITH BAKED ON DRY FILM LUBRICANT SHALL BE AS SPECIFIED IN THE FD
- 3. THE BOLT USED DETERMINES THE TORQUE REQUIREMENT FOR THE NUT. THEREFORE, ALTHOUGH A NUT MAY BE LISTED IN MORE THAN ONE COLUMN, IT SHALL BE TORQUED TO THE VALUE IN THE NUT COLUMN IMMEDIATELY TO THE RIGHT OF THE BOLT USED.
- 4. IF THE BOLT IS USED IN SHEAR AND A "TENSION" NUT IS USED, THE TORQUE REQUIREMENTS SHALL BE AS SPECIFIED IN TABLE 2. UNLESS OTHERWISE SPECIFIED IN THE FIELD OF DRAWING.
- 5. CASTELLATED NUT PROCEDURE:
 - A. TIGHTEN NUT WITH TORQUE WRENCH TO MINIMUM VALUE SPECIFIED IN TABLE.
 - B. IF SLOT IN NUT IS NOT ALIGNED WITH HOLE IN BOLT. CONTINUE TO TIGHTEN NUT UNTIL HOLE AND SLOT ARE ALIGNED.
 - C. IF SLOT IN NUT IS ALIGNED WITH HOLE IN BOLT, CONTINUE TO TIGHTEN NUT SO THAT IT MOVES A MAXIMUM OF ONE CASTLE OR 60° OF ROTATION. TORQUE SHOULD NOT EXCEED THE MAXIMUM VALUES SPECIFIED IN TABLE FOR THE APPLICABLE THREAD SIZE.
- 6. TORQUE VALUES FOR AN924 JAM NUTS USED ON FLARED AND FLARELESS FITTINGS IN BULKHEAD INSTALLATION SHALL BE PER MS33566. UNLESS OTHERWISE SPECIFIED ON THE FD, ALL OTHER JAM NUTS SHALL BE TIGHTENED 1/6 TO 1/3 TURN BEYOND THE POINT WHERE A SHARP RISE IN TORQUE IS FELT.
- 7. CAUTION NOTED FOR TITANIUM AND PASSIVATED CRES: TO PREVENT HEATING AND GALLING OF TITANIUM AND PASSIVATED CRES PARTS OR BOLTS, COAT THE BOLT THREADS WITH LUBRICANT QUALIFIED TO MIL-L-23393 OR MIL-L-46810 AND APPLY REQUIRED TORQUE WITH A HAND TOOL AT A RATE THAT WILL NOT CREATE HEAT. DO NOT USE A TORQUING (DRIVING) MACHINE.
- 8. SELF-LOCKING TK (TEMP LOK) BOLTS MANUFACTURED TO ANY OF THE STANDARDS SPECIFIED IN THE TABLE ABOVE SHALL USE THE SAME TORQUE VALUES AS APPLIED TO THESE STANDARDS.
- 9. TORQUE VALUES WITHIN TORQUE SYMBOLS SHALL HAVE A TOLERANCE OF ± 5%, UNLESS OTHERWISE SPECIFIED.

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Coating, Epoxy, VOC-Compliant MIL-C-22750

MIL-C-23398 Lubricant, Solid Film, Air-Cured, Corrosion Inhibiting

Fittings, Installation of Flareless Tube MS33566

MIL-L-46010 Lubricant, Solid Film, Heat Cured, Corrosion Inhibiting

MIL-T-81772 Thinner, Aircraft Coating

REQUIREMENTS 3.

ASSEMBLY TORQUE VALUES 3.1

Unless otherwise specified on the field of drawing, assembly torque values shall be as specified herein.

FIELD OF DRAWING (FD) CALLOUT 3.1.1

Special assembly torque requirements shall be indicated in the FD by a torque symbol consisting of a 0.62 dia. circle with diametrically opposed (top and bottom) arrowheads affixed by a leader to the nut end (preferred) or boit to be tightened. The assembly torque shall be shown within the symbol. Unless otherwise specified, torque is in inch lbs. and the tolerance on the torque value shall be ±5%. (See Figure 1a.) If the torque is specified at the nut end, but the nut end is inaccessible, then the torque may be applied at the head end of the bolt. Unless otherwise specified, the torque at the head end of the bolt shall be 10% higher than the torque specified for the nut. When a torque range is specified on the engineering drawing, the bolt, screw, or nut shall be torqued to a nominal value that is halfway between the lower and upper limits of the range.

If the specified torque for a nut is 100-160 IN LBS, then the nut shall be ex. torqued to 130 IN LBS.

ABSENCE OF SPECIFIED ASSEMBLY TORQUE VALUES 3.1.2

Sometimes bolts, screws, or nuts do not have assembly torque values or procedures for applying torque specified on the engineering drawing. In these cases. the torque values in a column of Table 2 corresponding to the strength and size of the bolt, screw, or nut shall be used.

NAS1204 has a tensile strength of 160,000 psi and a .2500-28 UNJF-3A thread. According to the bolt column of Table 2 corresponding to a tensile strength of 160,000 psi, the assembly torque for NAS1204 is 125 IN LBS.

If the assembly lorque values are unspecified and the size of the fastener is less than #10 or the tensile strength of the fastener is less than 125,000 psi, then the threaded parts shall be tight. The word tight means that the bolt, screw, or nut shall be firmly secured and that there shall be no relative movement between the attached parts.

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SUBJECT: CH53E/T64-415 Stability Analysis (1977)

AEG-Lynn February 7, 1977 cc: GM Douglass
AJ Fleischmann
RE Gaerttner
PD Hoffman
MC Hollenbeck
RL Miller
JD Stewart
JA Wilson
Letterbook
DRB

:781+594-4688

References:

- 1. EPN 64F643 (Proposed) T64 MFC N = Servo Redesign
- 2. CM No. (S/A) 5024 CH53E Rotor/Drive-Train Simulation for $N_{\rm f}$ Servo Redesign 12/1/76
- 3. CM No. (S/A) 5025 Drive-Train Parameters During Autorotation 12/21/76
- 4. CH53E/T64-415 Stability Analyses 7/16/76 Through 10/13/76
 - a. Initial Report
 - b. Supplements I Through VI
 - c. "Effects of Parameter Errors"
 - d. "Preliminary Runs with Revised Simulation"
- 5. T58-5/RSRA Rotor Governing Stability Analysis 6/15/76

Mr. W. M. Meyer, Manager T58/T64 Turboshaft Programs Building 34031

Summary

Revised simulations of the CH53E aircraft drive-train and rotor system were used to analyze system stability. The results are consistent with reported aircraft flight experience and with prior analyses. Use of a revised T64-415 engine P3-sensing hose would provide some stabilization of the 2-Hertz oscillations. However, it would not provide a complete problem solution. A power turbine governor time constant change to approximately three times its current value would provide such a solution.

Control and engine portions of the system simulation are currently being reviewed. The results will be used to spot check the current analysis and refine the requirements for the governor. Flight testing will be required to evaluate the speed of response change resulting from increases of the governor time constant.

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Conclusions

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- 1. The revised CH53E aircraft load system simulation along with previously used simulations of the T64-415 engines provides a good analytical model for the study of stability trends at critical 2-Hertz mode flight conditions.
- 2. The system behavior predicted by this model is consistent with reported test experience including the effect of small system changes and repeatability of divergent 2-Hertz instability.
- 3. The predictions of the model are expected to be conservative at flight conditions other than those which are critical for the 2-Hertz problem. Substitution of appropriately larger values of lag damping and aerodynamics damping coefficients would remedy this defect.
- 4. Introduction of P3-sensing lag by use of the revised P3-sensing hose would help to limit the magnitude of 2-Hertz oscillations. It would not eliminate the oscillations; nor would it be effective at all conditions of system tolerances. It would provide a temporary expedient which permitted further flight testing at critical 2-Hertz conditions, not a permanent problem solution.
- 5. A three-times increase of the Nf-governor time constant would recover the desired minimum levels of stability margin providing that further reductions of effective main rotor blade lag damping do not occur.
- 6. The governor change will result in a reduction of the system speed of response for noncollective compensated power demand changes. The effect is not expected to significantly impact on aircraft handling qualities. However, flight evaluation would be required.

Recommendations

- Continue with work effort now in process to refine the simulations of the engine and control system.
- 2. Use the resulting simulations to reanalyze 2-Hertz stability and refine the requirements for $N_{\rm f}$ governor changes.
- 3. Use the revised P_3 -sensing hose only as a temporary expedient solution to the 2-Hertz problem to permit flight testing until a permanent solution becomes available.

Discussions

Further predictions of the linear stability margins were made. These calculations employed the updated CH53E helicopter drive-train and rotor simulations which were presented in references (2) and (3). The predictions considered the full range of coupled engine power as well as autorotational operation.

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Discussions (Continued)

The new load system simulation differs from that considered in the 1976 stability analyses in the following respects:

- o the main rotor system is defined by a lumped-parameter schematic rather than by a transfer function
- o main rotor parameter values have been revised from those implied by the transfer function
- o minor levels of main rotor and tail rotor aerodynamic damping have been added
- drive-train and tail rotor parameter values have been revised.

The definition of the load system presented in reference (2) included values for two engine parameters which interact directly with the aircraft rotor system drive-train. Unfortunately, incorrect values were tabulated. PT, the power turbine rotor rotational movement of inertia, is 8.59 pound-feet-squared (3.204 inch-pound-seconds-squared). This is a revised value which differs from the value appearing in current engine documents. It was determined experimentally and corroborated by calculations. The correct value of PTS, the power turbine output shaft torsional spring constant, is estimated to be 83,000 inchpounds per radian rather than 303,000 inch-pounds per radian as tabulated in reference (2). The 303,000 value may be calculated from data presented in paragraph 3.23 of the T64-415 engine model specification. It corresponds to the measuring section of the external torque shaft but does not include the entire external torque shaft nor that section of the power turbine shaft which is contained within the engine. Experimental verification of the PTS value has been planned. The larger reference (2) value had been used in prior stability analyses. Stability analysis runs were made to define the impact of this error on the system stability margins. The calculation results indicated that the effect was negligible.

The main rotor lag damping coefficient provided in reference (2) was selected to "correspond to the critical high speed, high power condition" but was applied at all levels of engine power. Consequently, calculated levels of main and tail rotor resonance gain margin will be conservative at levels of engine power which do not correspond to the critical flight condition. Higher values may also be expected at other conditions of operation (e.g., hover or low speed flight) where the total levels of main rotor blade lag activity are more compatible with the capabilities of the lag dampers.

It was assumed that main rotor aerodynamic damping would vary linearly with total engine power through the two values provided in reference (2). In accordance with reference (2) instructions, lag damping was decreased by the amount of aerodynamic damping applied at each power level. It was noted that the level of aerodynamic damping defined by reference (2) is 15% of that which would be calculated based on the assumption that rotor torque demand varied as the square of rotor speed. The minimum expected level based on prior stability

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Discussions (Continued)

analysis experience is 40%. The defined aerodynamic damping values apparently also correspond to the critical flight condition and could be expected to be greater at other power levels or other conditions of flight.

A series of stability margin calculations were made for each of four configurations of the engine control system:

- o Series A Standard Control System
- o Series B Revised P3-Sensing Hose
- o Series C 4-Times Nf Governor Time Constant
- o Series D 3-Times N_f Governor Time Constant

Stability margin results over the power range are tabulated in Tables I, II, III and IV. All of the calculations are based on operation at 100% power-turbine speed and three engines at equal power levels.

Table I indicates that the lowest levels of stability margin at the main rotor resonance mode occur over the upper half of the available engine power range with the minimum margin occurring at normal rated power. The calculated level at NRP is very small but positive indicating that the system would be stable but subject to prolonged periods of slowly converging oscillations at rotor resonance frequency, if suitably disturbed. However, the margin is small enough so that normal system tolerance effects could frequently result in a negative stability margin and an unstable divergent pattern of oscillation. This indication of the analysis is entirely consistent with the reported flight testing results. The resonant frequency predicted by the analysis is approximately ½ Hertz higher than the nominal value reported from flight testing.

Stability margins at the tail rotor resonance mode decrease with increasing system power level and drop below the desired minimum level above normal rated power.

The system phase margin is excellent across the entire range of coupled power. It is lower for autorotational operation but still exceeds desired minimum levels. There does not appear to be a significant difference in autorotational stability between the outboard engines and the aft engine.

The calculation results at NRP (Case AO3) in Table I are very close to results obtained for the prior aircraft simulation as reported for Case 4O3 in reference (4)-c. The small differences are attributed to differences in the aircraft simulations.

Table II indicates the effects of adding P_3 -lag by using the revised P_3 -sensing hose. The nature of the P_3 -lag effect was discussed in reference (4)-b (Supplement III). The resulting effective P_3 -sensing time constant is sensitive

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Discussions (Continued)

to the level and rate of change of the P_3 signal. At the time constant breakpoint frequency it varies directly with the square root of oscillation amplitude and inversely with the square root of nominal P_3 level. This means that low effective time constant levels will be experienced during slow transient or at steady-state conditions for which low amplitudes of oscillation are present. The effective time constant will increase for rapid transients or increased magnitudes or frequencies of oscillation. Thus, the revised P_3 -sensing hose will tend to limit rather than eliminate oscillations at the 2-Hertz mode. The time constant level analyzed in the calculations of Series B corresponds to a P_3 amplitude of $\frac{1}{2}$ 1.5% of steady-state P_3 and the steady-state P_3 level which corresponds to each power level.

Tables III and IV indicate the effects of 4-times and 3-times increases of the $N_{\rm f}$ governor time constant. An increase factor of three is sufficient to provide the desired minimum level of gain margin at main rotor resonance. It also provides excellent levels of gain margin at tail rotor resonance. Note, though, that the phase margins and frequencies at gain cross-over have decreased significantly from those occurring for the standard control system.

The resulting phase margins are still quite adequate. The decrease indicates that the low frequency component of settling-out oscillations will be somewhat less damped than for a standard system.

Gain cross-over frequency is a rough index of the system speed of response for applied disturbances. High cross-over frequencies correspond to high speeds of response. The increased governor time constant will reduce the speed of response of the system. This effect will apply only for power demand changes that are not accompanied by corresponding changes of collective compensation signal to the fuel control Beta shaft. It may be noted that the gain cross-over frequencies of Table IV are approximately equal to those presented in reference (5) for T58-5 powered RSRA aircraft.

Tables II, III and IV indicate that autorotational stability is insensitive to P_3 sensing or N_f governor changes. The governor changes would result in lower speeds of response but this effect has little significance when the power turbines are de-coupled from the drive train.

Main fuel control block diagram definition testing is now in process at Hamilton Standard. The results of this testing could alter the transfer functions now used to simulate the dynamic behavior of the several control paths. Current simulations indicate that the principal dynamic effects occur at frequencies above those which are significant for engine/airframe interactions for all but the $N_{\rm f}$ error servo. That servo has dynamics at lower frequencies consistent with its specified time constant. Test results are not expected to materially change the control simulation. Some minor refinement of low frequency dynamics and the addition of less-significant high frequency dynamics is expected.

13 P7 2-14-77

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W. M. Meyer - February 7, 1977 - Page Six

Discussions (Continued)

Test data from recent transient testing of a T64-415 engine are also now being analyzed and applied to refinement of a transient simulation model of the engine system. These data will also be reviewed and applied to refinement of the linear engine simulation that is used for stability analyses.

Further stability analysis calculations will be made to evaluate the effects of control and engine simulation refinements as those refinements are defined.

E. W. Coldewey, Senior Engineer

T58/T64 Controls and Accessories Design

Building 34019 Extension 4857

/p

CH53E / TG4-415 LINEAR NF GOVERNING STABILITY ANALYSIS

TABLE I - BENCH-MARK CONDITIONS

- · 3 ENGINES OPERATING @ NF = 100 %
- . STANDARD CONTROL SYSTEM

CASE NO. SHP/ENGINE TOTAL SHP	A01 4645 13940	A02 4150 12450	A03 3646 10940	404 3/00 9300	405 2600 7800	406 2100 6300	A 07 1600 4800	A08 //00 3300	409 700 2100	A10 350 1050	A 11 C (COUPLEO)	A12 O AUTOROT: ENG 2	A 13 O A UTO 120T. ENG 1,3
GAIN CROSS OVER FREQ, RAD /SEC. PHASE MARGIN, DEG.	3.19 +68	3.22 +65	3.18 +64	3.12 +63	3.03 +63	2.87	2.66 +64	2.44 +64	2.19 +63	1,78 +68	,905 +93	5.87 +42	5.94 + 4 1
IST PHASE CROSS-OVER FREQ; LAD /SEC. GAIN MARGIN, DB.	/6.28 +.85	/5.79 + ,32	15.37	15.10	14,96	14.90	14.8z +2.98	14.22 + 4.8	14.66	14.68	14.93		
2NO PHASE CROSSIONER FREQ, RAD /SEL. GAIN MARGIN, DEL	37.68 +3.7	37. C5 +4. 8	37.62 +6.0	37.60 + 6.7	37.59 + 7.7	37.59 +8.9	37.59 +10.3	37.57	37.60 +/4.5	37.60 +17.3	37.61		

EWC 1-26-77

CH53E/TG4-415 LINEAR NF-GOVERNING STABILITY ANALYSIS

TABLE II - REVISED P3-SENSING HOSE

CASE NO. SHP/ENGINE TOTAL SHP	801 4645 13940	B02 4150 12450	B03 3646 10940	804 3100 9300	805 2600 780 0	806 2100 6300	E07 1600 4800	1308 1100 3300	809 700 2100	B10 350 1050	13/1 O (COUPLED)	B/2 O AUTOROT ENG 2	B13 O AUTORDT ENG1,3
GAIN CROSS-OVER FREQ, RAD/SEC. PHASE MARGIN, DEG.	3.15 +63	3.16 +61	3.12 +60	3.06 +57	2.9G +59	2.79 +60	2,59	2.37 +60	2.14 +60	1.72 +65	,900 +91	5.38 + 43	5.42 + 43
15T PHASE CROSS-OVER FREQ, RAD/SEC GAIN MARGIN, DB.	/6,42 + 3.33	/6.00 +2.90	15.61 +2.72	/5.37 +2.82	/5.24 + 3.41	15.17	/5./2 +5.6	15,02 + 7.2	14.95	/4.97 +12.2	15,21 +16.5		
ZND PHASE CROSS-OVER FREQ, RAG/SEG GAIN MARGIN, DB	37.84 + 5.4	37.79 + 6.0	37.73 +6.9	37.71 + 7.8	37.70 +8.7	37.70	37.69 +11.1	37.69 +/3.0	37.69 +15.2	37.69 +17.9	37.69 +21.9		

EW2 1-26-77

5-14-7 15 15-16-7 CH53E/TG4-415

LINEAR NE-GOVERNING STABILITY ANALYSIS

TABLE III

4x NF GOVERNOR TIME CONSTANT

CASE NO. SHP/ENGINE TOTAL SHP	C01 4645 13940	CO2 4150 12450	CO3 3646 10940	Co4 3100 9300	C05 2600 7800	2/00 2/00 4300	C07 1600 4800	CO8 //00 3300	C09 700 2100	C10 350 1050	C// (COUPLED)	C12 O AUTO ROT ENG 2	C13 O AUTOROT ENG1,3
GAIN CROSS-OVER FREQ, RAD /SEC PHASE MARGIN, DEG.	2.30 + 42	2.32 +40	2.29	2.27 + 38	2.20 +38	2./0	1.98 +40	1.84	1.69	1.42 +46	.80G +75	3.17	3,19
IST PHASE CROSS OVER FREQ, RAP/SEC GAIN MARGIN, PB	14.68	14,36	14.09 + 7.9	/3.9/ +8.0	/3.8/ +8.6	/3,77 +9.6	/3.72 +///o	/3.64 +/2.8	/3.58 +/5./	/3.59 +/8./	/3.78 + 22.3		_
2ND PHASE CROSS OVER FREQ, RAD ISEC GAIN MARGIN, DB	37.59 +15.6	37.55 + 16.5	37.52 +/7.6	37.50 +18.7	37.50 +/9.7	37.50 +20.7	37,50 +22,/	37.50 +24.0	37.50 +26.1	37.50 +28.9	37,51 .		

EWC 1-26-77

CH53E / TG4-415

LINEAR NF-GOVERNING STABILITY ANALYSIS

TABLE IV

3X NF GOVERNOR TIME CONSTANT

CASE NO. SHP/EMGINE TOTAL SHP	DO1 4645 13940	002 4150 12450	D03 3646 10940	004 3/00 9300	005 2600 7800	006 2100 6300	Do7 /600 4800	008	D09 100 2100	D10 350 1050	D O (COUPLED) O	DIZ O AUTOROT ENG. Z	DI3 O AUTOROT ENGI,3
GAIN CROSS OVER FREQ, RAD ISEC PHASE MAILGIN, DEG	2.52 +46	2,55 +44	2.55 +42	2.50 +42	2.42 +42	2.30	2./7	2.02	1.82	1.49	,843 +80	3.68 +42	3.70 +42
157 PHASE CROSS-OVER FREQ, RAD/SEC GAILL MARGILL, DB	14.84	14.50	14.21	14.02	13.92	13.88	13.82	13.74	13.69	13.70	14.74 +20.2		
2NO PHASE CROSS OVER FRED, RAD/CEE GAIN MARGIN, DB	37.60 +/3./	37.57 +14.0	37.53 +/5·/	37.51 +16.2	37.5/ +17.2	37.51 +/8.2	37.51 +/9.6	37.5/ +2/.5	37.51 +23.8	37.52 +26.5	37.52 +30.5		

EWC 1-26-77

13 1911 2-14-77 Sikorsky Aircraft Corporation 6900 Main Street, P.O. Box 9729 Stratford, Connecticut 06497-9129 (203) 388-4000



SEL-9369 07-AF-FA8509-0043

November 15, 2007

AFSOC A/8PP
Attn: Maj. Mike Stohler
100 Bartley Street
Suite 243 West
Hurlburt Field, FL 32544

Attention: Maj. Mike Stohler

Subject: Sikorsky Drawing Submittal in response to the USAF MH-53M Mishap Investigation

Reference: (a) Contract FA8509-05-C-0001, DD Form 1423-1, Contract Data Requirements List

Item A004, Technical Report - Study / Services

Enclosure (1): CD-ROM containing the following drawing 65350-07101.

The Contractor hereby submits Enclosure (1) in accordance with the requirements of Reference (a).

Sikorsky provides drawing 65350-07101 Revision M, FD Sheets 1 and 2, Revision K, FD Sheet 2 and 3, EO 41242 against Drawing 65350-07101 Revision B, FD Sheets 2 and 3, Revision A, FD Sheets 2 and 3.

All questions regarding this enclosure may be addressed to the undersigned at (203) 386-5382.

Very truly yours,

SIKORSKY AIRCRAFT CORPORATION

Michael A. Gugliotti

Engineering Team Lead, Aftermarket Engineering Platform

al A. Hugliott

Cc: Mr. Jim Sawinski, MH-53 Aero Engineer

Mr. Ray Goorah, MH-53J/M Project Engineer

Mr. Dan Smith, MH-53J/M Engineering

DECLARATION OF TECHNICAL DATA CONFORMITY

The contractor, Sikorsky Aircraft, hereby declares that, to the best of its knowledge and belief, the technical data delivered herewith under Contract FA8509-05-C-0001 is complete, accurate and complies with all requirements of the contract.

Date: 11/15/2007

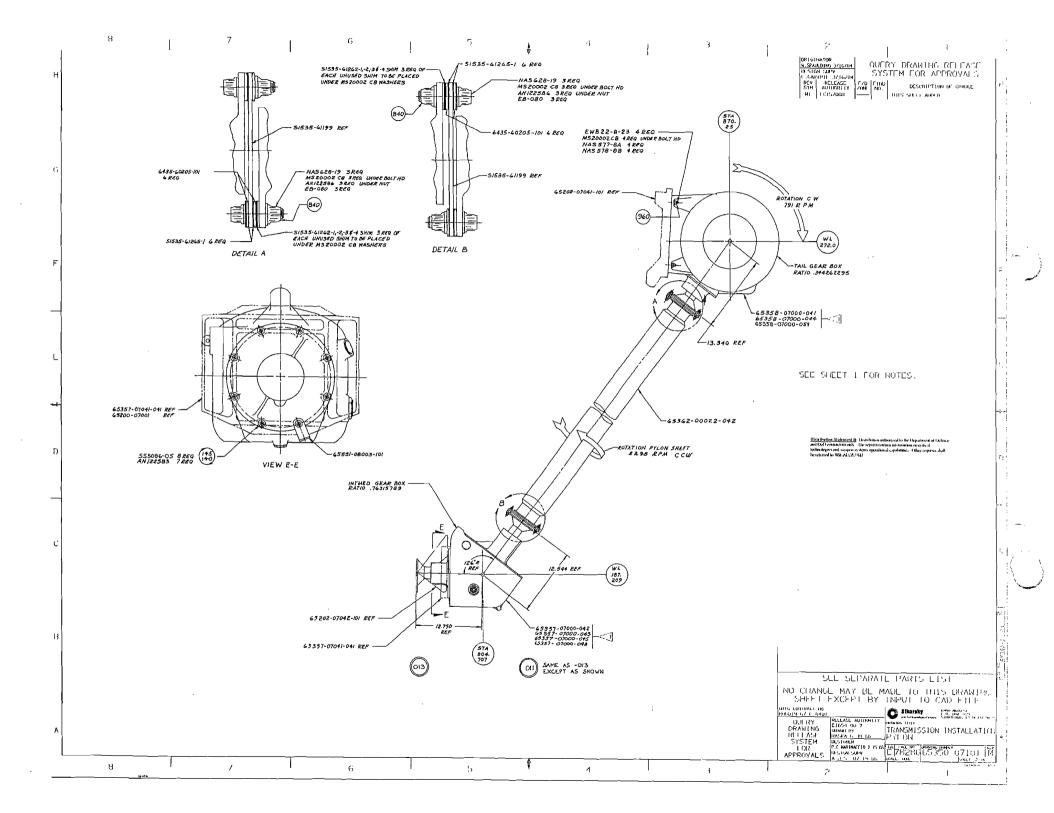
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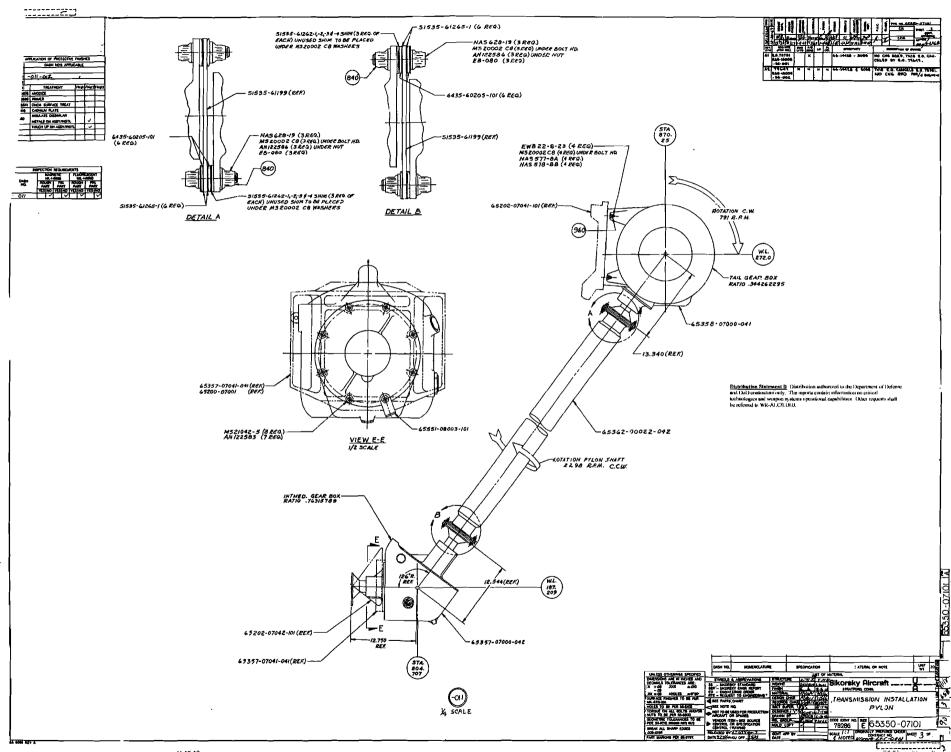
Michael A. Gugliotti

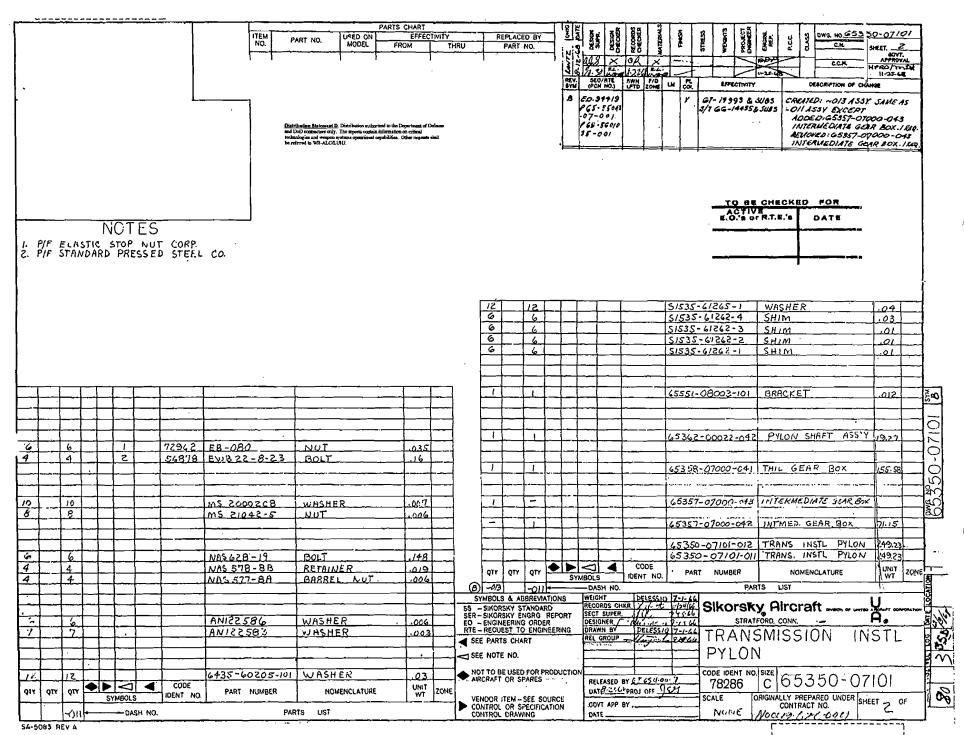
Engineering Team Lead,

Aftermarket Engineering Platform

A. Suglisti







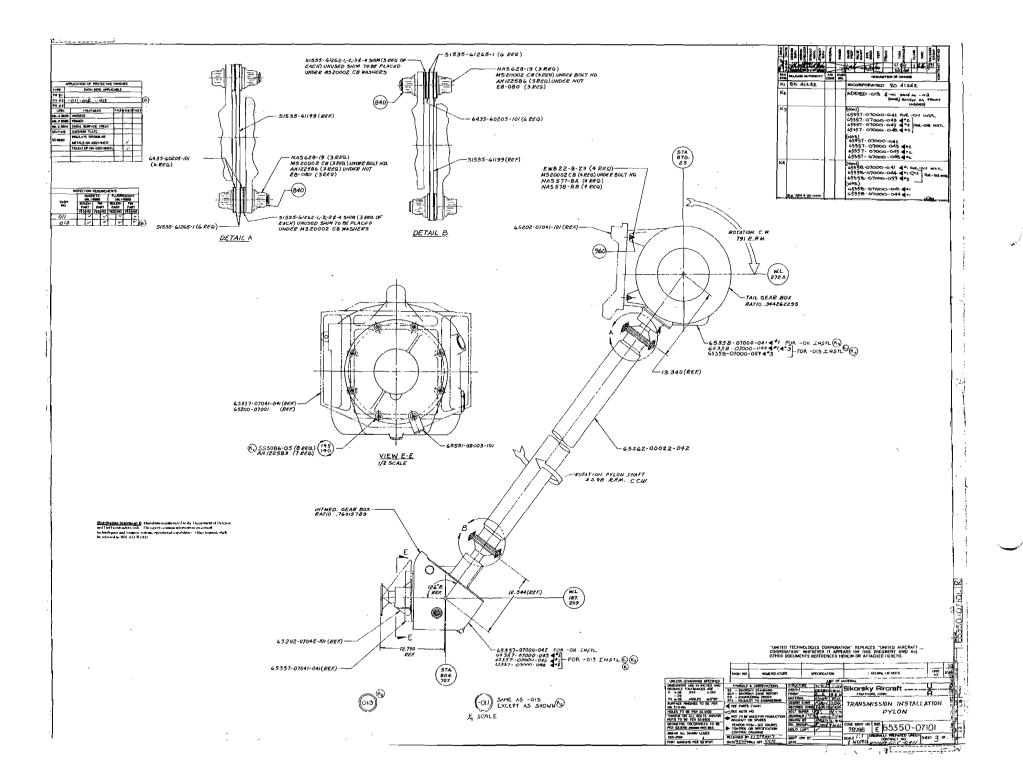
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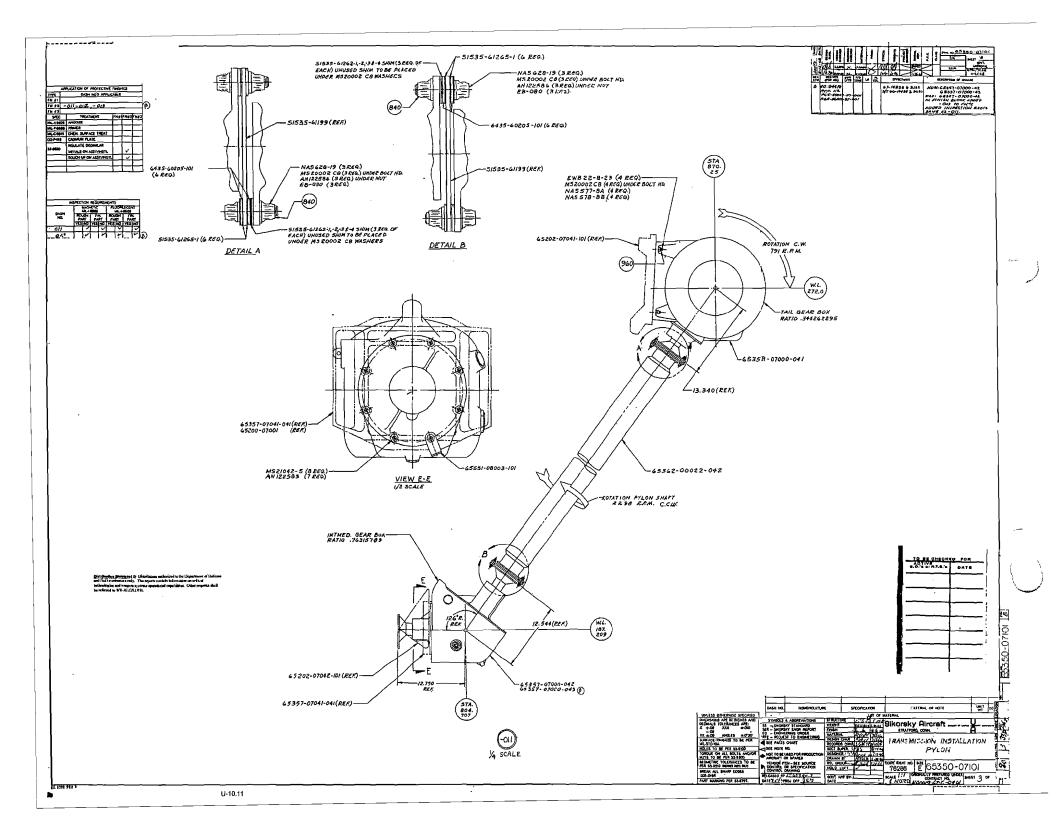
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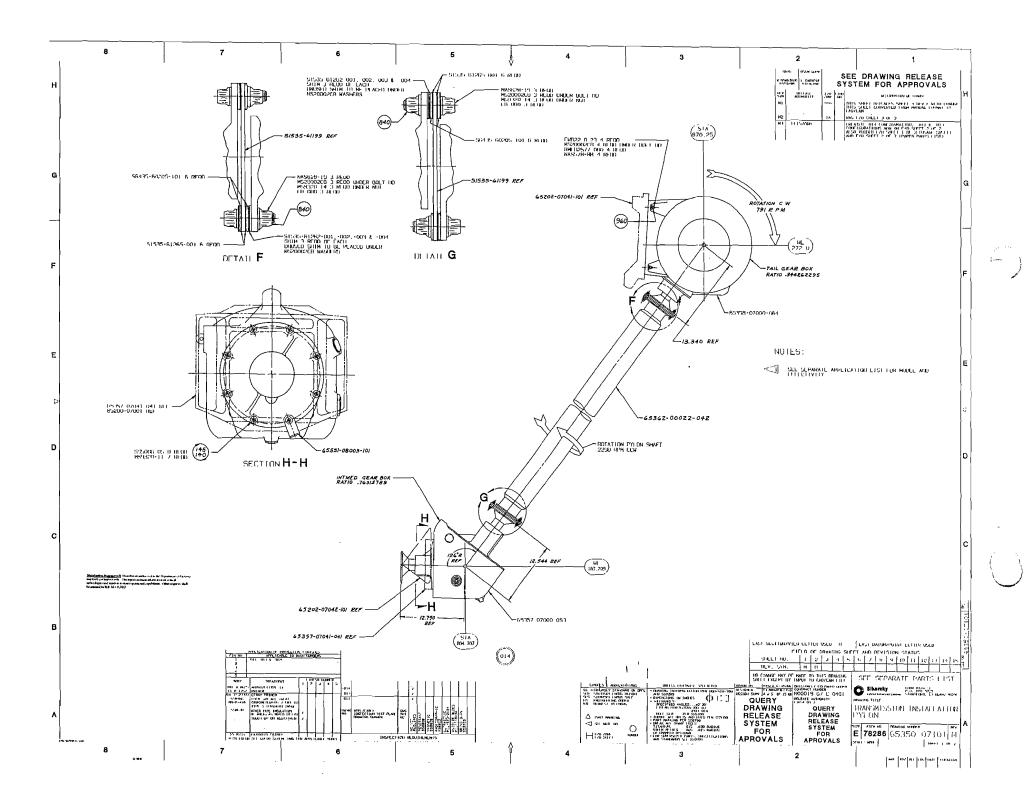
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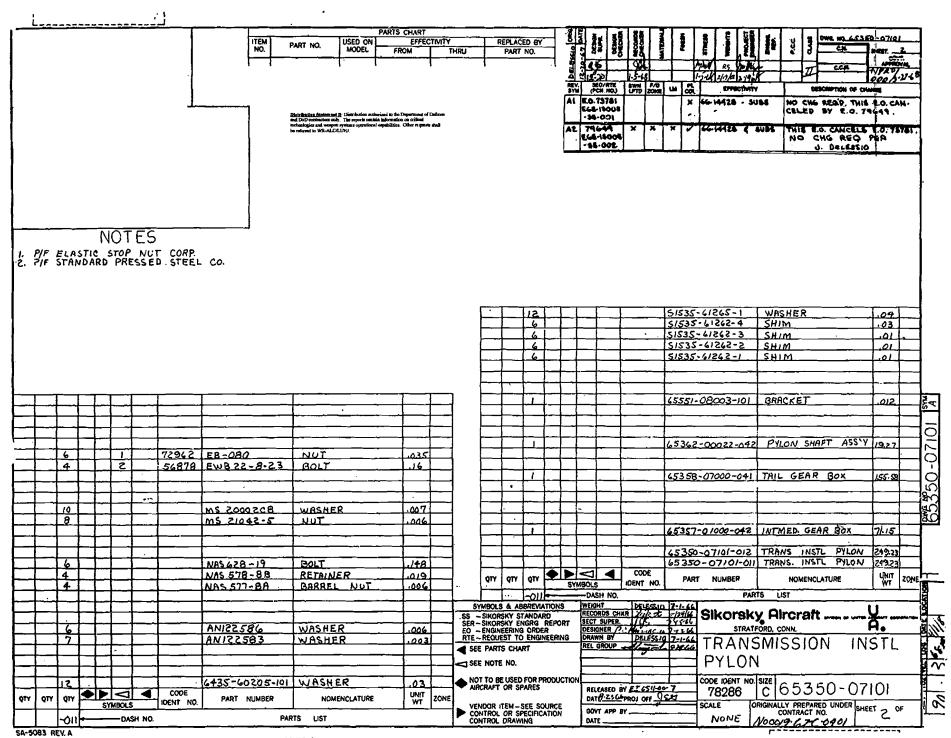


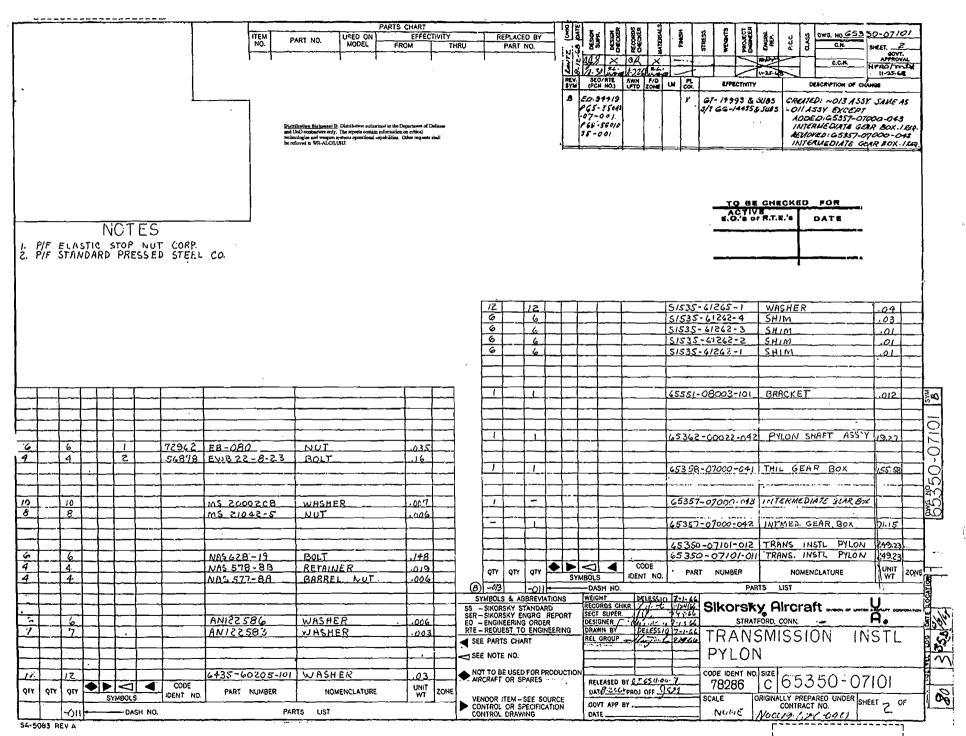


ENCLOSURE (1) CDRL A004 Technical Report – Study/ Services

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Warner Robins Air Logistic Center Engineering Report Aircraft 69-05794 Mishap 7 September 2007

<u>Background Information:</u> The crew experienced a problem in a hover after overshooting the desired landing zone. The pilot in command took the controls and executed a right turn to return to the landing zone. During the execution of the emergency landing the aircraft landed hard causing extensive damage to the airframe.

<u>Physical Evidence and Analysis:</u> This section presents observations of the physical evidence and in some cases a factual analysis of the significance of the evidence with the main area of concentration being the transmission system. Not all aircraft airframe and system discrepancies, or lack thereof, observed are discussed herein.

Discussion: Numerous parts from mishap aircraft S/N 69-05794 had been shipped to Sikorsky Aircraft Corporation (SAC) and then later to the Fleet Readiness Center (FRC) East at Cherry Point, N.C. for evaluation in an effort to determine a possible cause of the mishap. A full list of the parts shipped to SAC for evaluation can be found in Tab Q. Parts shipped to FRC East include: Intermediate Gear Box (IGB), Tail Gear Box (TGB), Tail Rotor Head, Tail Rotor Blades, #1, #2, # 3, #4, #5, #6, and # 7 Drive Shaft, Main Gear Box Tail Take Off Gear, IGB Mount Bracket, IGB Armor plate and mount brackets. A full report verifying material type and modes of failure has been submitted by SAC.

Components:

1) Intermediate Gear Box (IGB):

The IGB had been disassembled for evaluation. The center housing had cracked during the mishap and mechanical cuts were taken of the housing material to evaluate the nature of the crack. Two cracks were found in the IGB center housing 180° apart from each other. The location of the cracks, using aircraft coordinates, are in the top left quadrant and the bottom right quadrant. Each crack progressed through an IGB mount hole. The mount holes serve a dual purpose, not only to attach the input housing to the center housing but also to mount the IGB to the airframe. Investigation by Sikorsky Aircraft showed that the cracks were a result of ductile overload and that no pre-existing conditions such as casting anomalies, fatigue cracking or corrosion existed (ref. Sikorsky Metallurgical Report SEL-9364). Close examination of the holes showed that the top left hole threads had no signs of damage (no threads stripped in the housing) indicating that the housing had cracked and separated prior to removal of the stud. Threads in the bottom right hole were stripped in the housing where the stud had pulled partially out. Fretting was observed on the sealing bores of the center and input housings. The fretting was found on the left side

MH-53M, S/N 69-05794, 20071105

of the bore. Fretting generally occurs between two surfaces in contact under load subject to repeated relative motion between the surfaces. Fretting could induce fatigue cracking although additional metallurgical analysis by Sikorsky Aircraft of the center housing did not show signs of fatigue. The input and output gears were examined. Both gears showed damage to the teeth with the greatest damage common to the input gear. The majority of damage common to both gears was restricted to the tips (outside diameter) of the gear teeth. Additional damage existed on the input gear common to the face of the gear teeth and appears to be from abnormal wear. The input gear had up to .12 inch missing from the tip of the teeth towards the root of the gear. The output gear had a "shaving" (.01 - .03 material removed) of material off of the tips common to the majority of the teeth. One tooth common to the output gear had a distinct impression (witness mark) in the tip that appears to be from contact with the input gear. Magnetic Particle Inspection of the output gear revealed numerous cracks at the roots of the teeth, 23 out of 30 teeth (approximately 75 percent) exhibited root cracking. Destructive testing was not accomplished on either of the gears. The damage found in the IGB gears is consistent with the center housing separating from the input housing thereby allowing the gear teeth to disengage and grind the tips of each other. Additionally, a cracked center housing would allow the housing to expand causing a displacement between the input and output gears. The SAC report states "Most of the IGB gears teeth exhibited shearing and smearing damage at the crests due to skipping, in the drive direction" and that the damage to the gears "happened in a relatively short time as there was no evidence of fatigue". Gear skipping may have caused the transmission system to load and unload. This rapid application and removal of load could result in transient droop or overshoot of power turbine speed. The cracks at the roots of the output gear are likely due to sudden engagement of the gear causing a very high impact load.

The IGB is protected from ballistic rounds by armor plate. The armor covers the bottom and the lower sides of the IGB and is fabricated from .25 thick 6AL-4V Titanium plate per MIL-T-46077. It is attached to the IGB using two (2) brackets fabricated from .063 thick 4130 Normalized steel per MIL-S-18729. The brackets found on the mishap aircraft were fabricated from .071 thick steel with an equivalent to slightly reduced hardness than the drawing requirement. As stated earlier, analysis of the IGB input and output gears revealed a "shaving" of the tips of the gear teeth consistent with the center housing separating from the input housing. It was noted during the post crash investigation that rotation the tail rotor head showed a no-load continuity of the drive through the TGB, pylon shaft (#7), IGB, disconnect coupling, and the #6, #5, #4, and #3 driveshafts. It is evident that at some point after separating, the gears became re-engaged. The armor plate may have assisted with the reengagement of the gears and could have prevented total separation of the IGB since it is attached to both the input and output housing while spanning the center housing.

A drawing and Technical Order review of the IGB installation was conducted. A review of the IGB installation procedures contained in TO 1H-53(M)J-2-4 revealed the torque required for the mount nuts common to the center housing studs to be 200 inch-pounds. A subsequent review of the Sikorsky Aerospace drawing 65350-07101

revealed the torque required for the same nut/stud to be 140 to 145 inch-pounds. This conflict was due to a drawing change that occurred after release of the TO. The drawing was updated in June 1976 at which time it added the 140/145 inch-pound torque per EO 41242, this was a Class II change. The reason for the change was "To Prevent Nuts From Loosen Torque". Updates to drawings for Class I changes are normally accomplished through a proposed modification (e.g. Engineering Change Proposal (ECP)) that identifies changes to the system/end-item configuration that affect form, fit, function, or interface. Drawing numbers, part numbers, serial numbers, etc., as well as technical order changes, are reflected in the ECP. Upon receipt and review of the ECP, the configuration control authority convenes a configuration control board (CCB) to evaluate the change. If the board approves the change, the contractor, usually, is responsible for updating records, drawings, and technical data necessary to accurately reflect the current configuration. Updating should include the complete incorporation of the changes into the drawings, associated lists, part numbers, and engineering technical data.

A Class II change on the other hand, is typically reviewed for concurrence in classification by the local government representative. Unless a government representative is identified in the contract (normally a person from the procuring activity), the Contractor (or ECP originator) is responsible for assigning change classification. If the USAF has a sustainment contract with an OEM to deliver drawing updates, (currently there is not such a contract in place regarding the MH-53 Helicopter), the received drawings are put into the Joint Engineering Data Management Information and Control System (JEDMICS) without a technical review.

2) Tail Gear Box (TGB):

The TGB had been disassembled for evaluation. Unlike the IGB no cracks were found in the housing. The input and output gears were examined. Both gears showed damage to the teeth with the input gear showing a greater extent of damage. Very light marks from gear teeth impressions from the input gear could be seen on the drive side face of output gear teeth. Heavy damage was primarily common to the tips of the gears although severe wear can be seen on the face of numerous teeth on the input gear. Magnetic Particle Inspection showed the existence of two cracks common to the roots of the teeth on the TGB input gear. Neither gear had been destructively tested. The Sikorsky Metallurgical Report (ref SEL-9364) stated that the tooth damage was due to an overload event that happened in a relatively short time with no evidence of fatigue or of progressive long term failure mechanism.

A bearing was sent from Sikorsky to their supplier (MRC Bearings Inc) for testing. Part number for the bearing is SB1127-1. This bearing is the most outboard bearing common to the TGB housing. It was reported by Sikorsky that this bearing had made an unusual noise when tested by their supplier. Additional analysis of the bearing at Cherry Point revealed the following: Radial play and ID/OD dimensions were generally conforming. The bearing did not have any notable raceway degradation other than hard particle debris denting. No functional deterioration was

noted. The oil deposits on the cage and outer ring was contaminated with a fine black debris and the lands of the outer ring were stained black. The running surfaces (rings and rollers) were darkened but not as black as the lands. The OD of the outer ring showed a 360 degree blackened ring (suspect fretting wear but it is a bit different than classic fretting). Overheating was found in the bore of the TGB housing common to the installation location of the bearing. There was no evidence that the bearing contributed to the mishap.

3) Tail Rotor Head:

A visual examination was made of the Tail Rotor Head. There was no apparent damage noticed with the exception of the "crown" fitting (cam assembly). This fitting faces the TGB and is used to keep the tail rotor blade from rotating when the tail is folded. The fitting had rub marks on the outside diameter and had a cracked flange that appears to be from contact with the spindle assembly.

Additional discrepancies were found common to the keyed washer for the pitch change shaft. This washer shows that the pitch beam translated in advance of the pitch change shaft by approximately 20 degrees. This means that the shaft lagged or stopped and that the pitch beam continued to rotate another 20 degrees.

The Tail Rotor Head does not appear to have been a factor in the mishap.

4) #3 Drive Shaft:

A visual examination was made of the #3 Drive Shaft. The forward flange retention nut had separated from the shaft due to static tensile overload which allowed the shaft to disengage from the splined connection common to the #2 shaft. The nut threads were stripped. There was also damage to the internal gears common to the end fitting. All damage appears to be a result of sudden impact. This overload most likely occurred at the time of initial aircraft impact, drive to the Tail Gear Box ceased at this time. The lack of damage common to the tail rotor blades (see 8)) confirms this. No defects were noted that may have contributed to the mishap.

5) #1, #2, #4, #5, #6, # 7 Drive Shafts:

A visual examination was made of noted Drive Shafts. Other than minor circumferential scarring there were no notable defects found common to these drive shafts. No defects were noted that may have contributed to the mishap.

6) Main Gear Box:

An external visual examination revealed that the Main Gear Box had no notable defects. Gears rotated freely by hand. A teardown and examination of the internal components was completed by Sikorsky Aircraft and their primary MGB overhaul source during the week of Nov 7, 07. No additional defects were found that may have contributed to the mishap.

7) Main Rotor Head:

The Main Rotor Head was damaged significantly. An elastomeric bearing had separated into two pieces. Numerous pitch change rods and damper assemblies were damaged. One yoke assembly had fractured common to the upper and lower lugs. All of the damage observed is consistent with sudden impact forces. No notable defects were found that may have contributed to the mishap.

8) Tail Rotor Blades:

The Tail Rotor Blades exhibited either no apparent impact damage, or were bent in a spanwise direction commencing from the blade tip. Two of the tail rotor blades showed spanwise damage and can to be attributed to the separation of the tail section and final impact of the tail blades with the ground. Two of the blades showed nodamage at all. No deformation signature consistent with blade rotation was observed as there was no leading edge or tip cap damage on any of the blades. This is — consistent with the separation of the #2 and #3 Drive Shafts. No defects were noted common to the Tail Rotor Blades that may have contributed to the mishap.

James Sawinski Aerospace Engineer WR-ALC 580 ACSSS/GFEAD (478) 327-6950 H53 ISSC Evaluation of Submitted Mishap Parts for Air Force MH-53M Aircraft 69-05794 Summary of findings as of 12/20/07

The USN H53ISST was asked to evaluate a group of dynamic components and drive system components from AF mishap aircraft MH-53M, 69-05794. The submitted items were:

Tail Rotorhead with Blades
Tail gearbox
Intermediate Gearbox
Tail Driveshafts Numbers 3 & 7
Main Gearbox Tail Drive Output Gear

- 1. Tail Rotorhead was examined and no anomalies were noted that would prevent normal function. The sleeves and spindles were intact and could be freely rotated. All pitch change links and the pitch beam were attached. The tail rotor positioning cam showed rotational damage and had a broken lobe. When received the tail rotor blades had been removed from the tail rotorhead but it is understood that they were attached at the site of the mishap. The tail rotor blades were intact and relatively free of damage indicating a low energy impact and low to no rpm impact. All damage noted was consistent with these small impact forces.
- 2. The Tail Gearbox (TGB) was examined. The gearbox had been disassembled prior to arriving. Both the input and output gears showed a large amount of damage. There were numerous chips within the gearbox housings. The driven side of both gears showed two distinct scuffing patterns, one on the high side of the tooth flank and the one on the low side. The middle of the teeth, where normal contact occurs, was relatively free of damage except for debris denting. The top of most of the teeth of both gears had heavy amounts of damage. The non-driven side of both gears had heavy scuffing indicative of a lack of backlash or the gears being backdriven. The bearings were examined and only debris denting was noted. The gearbox was reassembled using existing shims. Drive continuity was evident even with the large amount of tooth damage. A pattern check was made and showed normal mid tooth contact. The gears showed no evidence of running out of mesh and appeared to be capable of transmitting torque at time of impact.
- 3. The Intermediate Gearbox (IGB) was received in a disassembled state. Extensive damage of all the gear teeth was noted on both gears. A large amount of metal debris remained in the housings. The input housing mounting studs located on the forward side on the IGB center housing showed various states of failure. All of the damage to the studs was consistent with impact related overload. The Center Gearbox housing had been sectioned by Sikorsky at an area where the housing had a crack. The crack was due to overload. A casting anomaly was noted in the threaded hole for the #1 stud. The anomaly was a sand inclusion that would have exceeded acceptance criteria. It is not thought that this anomaly is related to the cracking of the gearbox housing or the mishap. Both of the gears in the IGB showed damage to the teeth indicative of the gears coming out of mesh

and over-riding each other. It is considered that this would have occurred during impact when the gearbox housing split open. No cause for the opening of the gearbox was seen that was thought to have occurred prior to impact. The drive side of the gears showed a normal running pattern.

- 4. The #3 and the #7 tail drive shafts were examined. The #3 shaft forward flange retention nut had separated due to static overload. The #7 shaft was relatively undamaged. Driveshafts were capable of transmitting torque until time of impact. The number 3 driveshaft was subjected to impact force severe enough to cause static overload of the retention nut at which time the rest of the tail drive system would have been undriven.
- 5. Conclusions. All damage noted is considered related to impact forces and no causal factors were seen for the items submitted.

Bill Hood H53 ISST.2 Senior Rotors Engineer ISSC Cherry Pt. NC 252-464-5650 William.e.hood@navy.mil P 021620Z JAN 08 ZYB

FM COMNAVAIRSYSCOM PATUXENT RIVER MD//DRPO// TO AFSOC HURLBURT FLD FL//PMA// INFO OCALC TINKER AFB OK/LPARP// COMNAVAIRSYSCOM PATUXENT RIVER MD//DRPO/4.4.3.2//
//NO4790// MSGID/GENADMIN/COMNAVAIRSYSCOM PAX DRPO// SUBJ/MH-53J EI FINAL REPORT//
REF/A/MSG/COMNAVAIRSYSCOM PATUXENT RIVE/021810ZOCT2007// REF/B/MSG/COMNAVAIRSYSCOM
PATUXENT RIVE/101820ZOCT2007// REF/C/DOC/COMNAVAIRFORINST 4790.2 CH-1/01MAY2006//
REF/D/DOC/OPNAVINST 3750.5C/21JUN2005// REF/E/DOC/OPNAVINST 5102.1C/01NOV2001//
REF/F/DOC/NA 02B-105AJB-6-2/01FEB2006// REF/G/DOC/NA 02B-105AJB-6-1CHG 3/01MAR2007//
NARR/REF A IS EI REQUESTING MESSAGE REF B IS EI PRELIMINARY REPORT REF C IS NAVAL
AVIATION MAINTENANCE PROGRAM INSTRUCTIONS REF D IS NAVAL AVIATION SAFETY INSTRUCTIONS
REF E IS MISHAP INVESTIGATION INSTRUCTIONS REF F IS T64 DEPOT MAINTENANCE MANUAL REF G
IS T64 INTERMEDIATE MAINTENANCE MANUAL// POC/LUCAS, CHRIS/-/NAVAIRDEPOT CHERRY PT
NC/LOC:H53ISST.6 /DSN:451-7127/TEL:252-464-7127// RMKS/THIS MESSAGE WAS AUTO GENERATED
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- 1. H53ISST.6/65923
- 2. F44170-07-366
- 3. AIRCRAFT T/M/S: N/A, BUNO: 000000, NOMENCLATURE: T64-GE-100 TURBOSHHAFT ENGINE, P/N: 6063T02G01, S/N: 261008, LOT/BATCH NR: NA, NSN: , CONTRACT NR: N/A, WUC: 22000
- 4. NAVAIRDEPOT CHERRY PT NC
- 5. ICN: WC2EI-T64-0009-07M
- 6. TIME SINCE NEW: UNK TIME SINCE REWORK: 892.9 7. LAST REPAIR DATE: NA 8. BACKGROUND: ENGINE WAS INVOLVED IN AIRCRAFT HARD LANDING. AIR FORCE MISHAP SAFETY BOARD REQUESTED INVESTIGATION OF ENGINE FOR OPERATIONAL CAPABILITY. REF A REQUESTED EI. REF B ASSIGNED EI AND PROVIDED SHIPPING INSTRUCTIONS IN ACCORDANCE WITH REF C THROUGH E.
- 9. DESCRIPTION OF FINDINGS: A. ENGINE WAS EXAMINED AS RECEIVED. NO LOG BOOK WAS PROVIDED WITH THE ENGINE. THE ENGINE WAS INSTALLED IN A HORIZONTAL MAINTENANCE STAND AND A BORE SCOPE WAS USED TO INSPECT THE INLET AND EXHAUST. NO FOD DAMAGE WAS SEEN ON THE COMPRESSOR OR 4TH STAGE TURBINE BLADES.
- B. THE GAS GENERATOR AND POWER TURBINE ROTATED FREELY WITH NO UNUSUAL NOISES.
- C. THE VARIABLE GEOMETRY SYSTEM WAS INSPECTED FOR RIG AND FREEDOM OF MOVEMENT. THE FEEDBACK CABLE ARM ON THE FUEL CONTROL WAS STIFF WHEN EXERCISED BY HAND BUT MOVED TO POSITION AS REQUIRED WHEN OPERATED BY THE VARIABLE GEOMETRY ACTUATORS.
- D. THE FEEDBACK CABLE RIG WAS CHECKED WITH THE RIG PIN AND FOUND TO BE AT NOMINAL RIG.
- E. THE VARIABLE GUIDE VANE SCHEDULE WAS CHECKED. RESULTS ARE AS FOLLOWS: IGV OPEN: 10 MINUTES OUT OF TOLERANCE LEFT SIDE, 5 MINUTES OUT OF TOLERANCE RIGHT SIDE IGV CLOSED: 10 MINUTES OUT OF TOLERANCE LEFT SIDE, IN TOLERANCE ON RIGHT SIDE. STAGE ONE OPEN: IN TOLERANCE LEFT SIDE, 45 MINUTES OUT OF TOLERANCE RIGHT SIDE. STAGE ONE CLOSED: 30 MINUTES OUT OF TOLERANCE LEFT SIDE, 1 DEGREE 30 MINUTES OUT OF TOLERANCE RIGHT SIDE. STAGE TWO OPEN: IN TOLERANCE LEFT SIDE, IN TOLERANCE RIGHT SIDE. STAGE TWO CLOSED: 1 MINUTE OUT OF TOLERANCE LEFT SIDE, IN TOLERANCE RIGHT SIDE. STAGE THREE OPEN: IN TOLERANCE LEFT SIDE, IN TOLERANCE RIGHT SIDE. STAGE 3 CLOSED: 15 MINUTES OUT OF TOLERANCE LEFT SIDE, 45 MINUTES OUT OF TOLERANCE RIGHT SIDE. STAGE 4 OPEN: IN TOLERANCE LEFT SIDE, IN TOLERANCE RIGHT SIDE. STAGE 4 CLOSED:
- 5 MINUTES OUT OF TOLERANCE LEFT SIDE, 10 MINUTES OUT OF TOLERANCE RIGHT SIDE.
- F. THE FUEL CONTROL FUEL DENSITY SELECTOR WAS SET TO THE NUMBER 6 SETTING.
- G. THE FLOW DIVIDER FILTER BOWL WAS REMOVED AND INSPECTED. A SAMPLE OF FUEL WAS RETRIEVED FOR ANALYSIS AND THE FILTER INSPECTED. NO ABNORMAL FINDINGS NOTED.
- H. THE CHIP DETECTOR WAS INSPECTED. A SLIGHT AMOUNT OF SLUDGE COVERED THE TIP.
- I. THE ENGINE WAS INSTALLED IN THE TEST CELL. ALL SYSTEMS PERFORMED NORMAL DURING A MOTORING CHECK. THE GUIDE VANES MOVED TO THE CAMBERED POSITION (CLOSED) AND THE ENGINE

TURNED WITH NO ABNORMAL NOISES TO MAXIMUM STARTER SPEED, APPROXIMATELY 5000 RPM. THE ENGINE WAS ALLOWED TO COAST DOWN. AT APPROXIMATELY 2000 RPM THE ENGINE VIBRATED BACK AND FORTH IN THE STAND WITH MAXIMUM MOVEMENT AT THE TAIL PIPE. HOWEVER, THIS DID NOT REGISTER ON THE VIBRATION PICKUPS AS AN OUT OF LIMITS VIBRATION. THE VIBRATION COULD BE SEEN AS THE ENGINE MOVED BACK AND FORTH AT THE TAIL PIPE. THE TYPICAL ENGINE DOES NOT DO THIS, BUT IT IS POSSIBLE TO PHYSICALLY GRASP THE TAILPIPE AND SHAKE THE ENGINE WHILE INSTALLED IN THIS TEST STAND. SINCE THIS BEHAVIOR OF AN ENGINE HAS NOT BEEN WITNESSED TO THIS DEGREE THE DECISION WAS MADE NOT TO START THE ENGINE DUE TO THE POSSIBILITY OF DAMAGING THE ENGINE OR TEST CELL OR LOOSING INFORMATION RELATED TO THE AIRCRAFT HARD LANDING.

- J. THE ENGINE WAS DISASSEMBLED LAW REF A AND B.
- K. THE FUEL CONTROL WAS REMOVED AND TESTED ON THE FUEL CONTROL TEST STAND. ALL PARAMETERS WERE FOUND TO BE WITHIN LIMITS.
- L. THE POWER TURBINE WAS REMOVED AND A RUN OUT CHECK WAS PERFORMED ON THE ASSEMBLY. THE RUN OUTS WERE WITHIN LIMITS. THE POWER TURBINE DRIVE SHAFT AND DISKS WERE CHECK BALANCED AND FOUND TO BE WITHIN LIMITS. THE POWER TURBINE FORWARD SPLINES WERE INSPECTED FOR WEAR AND/OR DAMAGE AND FOUND TO BE WITHIN LIMITS.
- M. THE GAS GENERATOR TURBINE ROTOR WAS REMOVED AND CHECK BALANCED. THE ROTOR BALANCE WAS WITHIN LIMITS.
- N. THE STAGE ONE TURBINE BLADE TIPS EXHIBITED HEAVY METAL BUILD UP DUE TO CONTACT WITH THE STAGE ONE TURBINE SHROUDS. THE SHROUDS EXHIBITED HEAVY RUB FROM APPROXIMATELY 4 OCLOCK TO 7 OCLOCK. THE STAGE ONE STATIONARY AIR SEAL EXHIBITED MODERATE WEAR FROM THE STAGE ONE ROTATING AIR SEAL FROM APPROXIMATELY 4 OCLOCK TO 7 OCLOCK. THE INNER BALANCE PISTON SEALS HAD A SIMILAR APPEARANCE. THE STAGE 2 TURBINE BLADES HAD VERY SLIGHT METAL BUILDUP WITH MODERATE RUB ON THE STAGE 2 TURBINE SHROUDS, AT THE 4 OCLOCK TO 7 OCLOCK POSITIONS.
- O. THE COMPRESSOR CASES WERE REMOVED. NO ABNORMALITIES WERE SEEN ON THE COMPRESSOR ROTOR, BLADES, CASES, OR VANES.
- P. THE TORQUE SENSOR SHAFT WAS INSPECTED FOR MISALIGNED SENSOR AND REFERENCE TEETH. THE RUN OUT BETWEEN TEETH WAS FOUND TO BE WITHIN LIMITS.
- Q. ALL THE MAIN BEARINGS WERE INSPECTED. THE NR 1 BEARING HAD NO DISCREPANCIES. THE NR 2 BEARING SHOWED SLIGHT DISCOLORATION BUT NO OTHER DISCREPANCIES. THE NR 3 BEARING HAD WHAT APPEARED TO BE SLIGHT INSTALLATION OR REMOVAL DAMAGE ON THE INNER RACE EDGE. THE NR 4 BEARING HAD NO DISCREPANCIES. THE AFT DIFFERENTIAL BEARING HAD INDICATIONS (VISIBLE SHINE OF NO APPARENT DEPTH) OF LOADING TO ONE SIDE OF THE RACEWAY.
- R. A RUNOUT WAS PERFORMED ON THE GAS GENERATOR ASSEMBLY (COMPRESSOR MATED TO TURBINE). ALL RUNOUTS WERE WITHIN REF F REQUIREMENTS.
- S. THE COMBUSTION CHAMBER AND FRAME AND NR 2 AND 3 BEARING SUPPORT WERE INSPECTED WITH A COORDINATE MEASUREMENT MACHINE FOR FLANGE/BEARING BORE ALIGNMENT. NO BEARING BORE MISALIGNMENT WAS DETECTED.
- 10. CONCLUSIONS: THOUGH THE ENGINE WAS NOT OPERATED ON THE TEST CELL IT IS APPARENT THAT THIS ENGINE WAS CAPABLE OF OPERATION AS REQUIRED. NO DISCREPANCIES WERE IDENTIFIED DURING DISASSEMBLY WHICH WOULD PREVENT NOMINAL OPERATION OF THE ENGINE. THE VANE ANGLES ARE NOT SUFFICIENTLY OUT OF TOLERANCE TO CAUSE COMPRESSOR OPERABILITY PROBLEMS. THE RUB ON THE TURBINE SHROUDS AND SEALS IS CONSISTENT WITH TURBINE ROTOR SHIFT AND/OR LOSS OF RUNNING CLEARANCE. THIS MAY BE THE RESULT OF LOADING DUE TO HIGHER THAN NORMAL G FORCE RELATED TO THE HARD LANDING. DURING THE LOADING THE CLEARANCES COULD NOT BE MAINTAINED AND THE BLADES AND SEALS MADE CONTACT WITH THEIR ASSOCIATED SHROUDS AND HONEYCOMB. CLEARANCE CLOSURE IS ALSO EXPECTED IN THIS AREA OF THE T64 DUE TO THE NUMBER 3 OIL DAMPENED BEARING AND THE LOSS OF BEARING CLEARANCE TO THE SUPPORT HOUSING DURING G LOADING. ADDITIONALLY, VISUAL CHARACTERISTICS (SHINE AND LACK OF SOOT OR CONTAMINANT DEPOSITS) OF THE RUB ON THE SEALS AND SHROUDS INDICATES THE ENGINE DID NOT OPERATE FOR AN EXTENDED AMOUNT OF TIME FOLLOWING THE RUB EVENT. THE ROTATING COMPONENTS IN BALANCE AND THE RUN OUTS OF THE SHAFTS AND TORQUE SENSOR SHAFT INDICATES THAT THE ROTOR GROUPS DID NOT SUSTAIN LOADS TO CAUSE PERMANENT DEFORMATION. CONSIDER BEARING FINDINGS TO BE NOMINAL FOR AN IN-SERVICE ENGINE. CONSIDER THE ENGINE VIBRATION WITNESSED DURING MOTORING TO BE UNRELATED TO MISHAP

EVENT. THERE IS NO EVIDENCE TO SUPPORT ENGINE VIBRATION DURING OPERATION PRIOR TO MISHAP, I.E. CRACKS IN VARIOUS LINE/HOSE BRACKETS OR EXCESSIVE WEAR ON MATING PARTS 11. RECOMMENDATIONS: NA 12. RELATED INFORMATION: GE AVIATION WAS CONTACTED TO PROVIDE INSIGHT INTO THE ENGINE VIBRATION DURING THE START ATTEMPT. THERE ANALYSIS INDICATES A VIBRATION MODE AT 2569 RPM WHICH RESULTS IN MAXIMUM AMPLITUDE AT THE ENGINE TAILPIPE. ADDITIONALLY, FURTHER OBSERVATION OF OTHER ACCEPTED ENGINES REVEALED THIS MODE BUT WITH LESS DISPLACEMENT AT THE TAILPIPE THAN THE MISHAP ENGINE. FST WILL MONITOR THIS MODE AND REPORT ANY FURTHER DEVELOPMENTS IF NECESSARY. AIB REQUESTED EXPLANATION OF T64 ENGINE GOVERNING PRINCIPALS OF OPERATION. THE T64 FUEL CONTROL UTILIZES A FLYWEIGHT GOVERNOR SYSTEM WHICH ACCEPTS A PHYSICAL RPM SIGNAL FROM A ROTATING FEEDBACK CABLE WHICH IS ATTACHED BETWEEN THE CONTROL AND AIRCRAFT NOSE GEARBOX. THE GOVERNOR FLYWEIGHTS ADJUST FUEL FLOW TO THE ENGINE (WHEN IN NF GOVERNING MODE) BASED ON THEIR CENTRIFUGAL MOVEMENT AT CHANGING SPEEDS. THE MOVEMENT OF THE FLYWEIGHTS ADJUSTS FUEL METERING VALVES WHICH SUPPLY FUEL TO THE ENGINE. IF THE HELICOPTER ROTOR HEAD SLOWS THE GOVENOR SLOWS WHICH DRIVES THE FLYWEIGHTS INWARD. THIS MOVEMENT CHANGES THE FUEL VALVE TO ALLOW MORE FUEL INTO THE ENGINE TO SPEED NG AND HENCE PROVIDE MORE COMBUSTION GAS TO THE POWER TURBINE WHICH WILL INCREASE TORQUE/ NF SPEED ON THE DRIVE SYSTEM. AS THE SPEED OF THE HELICOPTER RECOVERS FROM THE SLOW DOWN THE FLYWEIGHTS RETURN TO EQUILIBRIUM AND SCHEDULE THE NECESSARY FUEL FLOW TO MAINTAIN THE DESIRED HELICOPTER ROTOR SPEED. THIS CYCLIC OPERATION IS SMALL UNDER NORMAL CONDITIONS AND DAMPED. THIS RESULTS IN STEADY STATE ENGINE OPERATION HENCE A CONSTANT NF SPEED. THE CONTROL ALSO COMPUTES LOAD CHANGES AND ANTICIPATES THE CHANGE SUCH THAT ROTOR DROOP/SLOWING IS NOT SEEN BY THE PILOT UNDER NORMAL FLIGHT CONDITIONS. THE SYSTEM IS DESIGNED TO REACT TO NORMAL HELICOPTER FLIGHT OPERATIONS WHICH WERE DETERMINED IN DEVELOPMENT AND ANY SUBSEQUENT MODELING OR TESTING. IF THE GOVERNING SYSTEM IS EXPOSED TO TRANSIENT CONDITIONS WHICH ARE OUTSIDE OF THE DESIGNED/TESTED PARAMETERS ITS ABILITY TO REACT WITH PREDICTABLE RESULTS MAY BE COMPROMISED. IF AN OUTSIDE INFLUENCE EXISTED SUCH THAT THE HELICOPTER ROTOR SYSTEM WAS SUBJECTED TO A CYCLIC LOADING AND UNLOADING THE GOVERNOR WOULD REACT TO EITHER REDUCE FUEL FLOW TO THE ENGINE OR INCREASE FUEL FLOW TO THE ENGINE AS NECESSARY BASED ON HELICOPTER ROTOR SLOWING (DROOPING) OR ACCELERATING PASSED THE NF GOVERNOR SET POINT. THE CONTROL IS CAPABLE OF HANDLING SUCH INPUTS TO A POINT AS DESIGNED, BUT IF THE CYCLIC INPUT IS AT A FREQUENCY NOT ASSOCIATED WITH THE DESIGN OF THE GOVERNOR, THE GOVERNOR AND HENCE THE ENGINE ROTATING SYSTEM MAY NOT REACT WITH PRECISION TO OFFER A STEADY NF AND MAY IN FACT DIVERGE. IDENTIFICATION OF THE MODES/INPUTS AT WHICH THE GOVERNOR MAY DIVERGE WOULD NEED TO BE PERFORMED BY THE ENGINE AND AIRCRAFT OEM.

- 13. PENDING ACTIONS: NA
- 14. THIS IS CONSIDERED CLOSING ACTION ON EI RCN: F44170-07-366, INVESTIGATION CONTROL NUMBER WC2EI-T64-0009-07M.//

Sikorsky Aircraft Corporation 6900 Main Street- P.O. Box 9729 Stratford, Connecticut 06497-9129 (203) 386-4000



December 21, 2007

SEL-9396 07-AF-FA8509-0045

WR-ALC/LUHJE 235 Byron Street Suite 19A Robins AFB, GA. 31098-1622

Attention:

Ray Goorah, MH-53J/M Project Engineer

Subject:

Contract FA8509-05-C-0001, MH-53J/M Integrated Product Team Engineering

Support

Reference:

(a) Contract FA8509-05-C-0001, DD Form 1423-1, Contract Data Requirements List

Item A004, Technical Report - Study / Services

Enclosure: (1) Sikorsky Aircraft teardown analysis of USAF MH-53M Mishap aircraft Main Gearbox

The Contractor hereby submits Enclosure (1) in accordance with the requirements of Reference (a).

The information contained in Enclosure (1) provides the results of the teardown analysis of a Main Gearbox Assembly, P/N 65351-11500-056. This assembly was installed on a USAF MH-53M aircraft, A/C 69-05794, while it encountered a hard landing mishap at Eglin AB, FL.

The enclosed Sikorsky proprietary data and intellectual property is provided voluntarily and in strict confidence at the request of the United States Air Force (USAF), and is accepted on that basis with the express agreement that this data will be restricted to the official use of the USAF and will not be released to any person outside the USAF without the prior written consent of Sikorsky Aircraft Corporation.

FOIA Exemption: This data is furnished in confidence and subject to exemption under subsection (b) of 5 USC 552.

DECLARATION OF TECHNICAL DATA CONFORMITY

The contractor, Sikorsky Aircraft, hereby declares that, to the best of its knowledge and belief, the technical data delivered herewith under Contract FA8509-05-C-0001 is complete, accurate and complies with all requirements of the contract.

Date: 12-19-2007

Name and Title of Authorized Official:

Ralph D. Brunks Jr

H-53/H-60 USAF Program Engineering

Manager

ENCLOSURE (1) CDRL A004

Sikorsky Aircraft Teardown Analysis of USAF MH-53M Mishap Aircraft Main Gearbox As part of the Mishap Investigation of MH-53M, A/C 69-05794, Sikorsky Transmissions Engineering evaluated the Main Gearbox Assembly, P/N 65351-11500, S/N A16-426. The evaluation results are detailed below.

Main Gearbox Assembly, P/N 65351-11500-056

The evaluation was conducted on 7 November 2007, at Overhaul Support Services (OSS), located at 18 Connecticut South Drive, East Granby, CT. Sikorsky employees, Chris Lowenstein, Alex Smith and William Meltzer were present during the gearbox teardown and evaluation. The controlled teardown/evaluation was performed per EI No.: E65D-725-35-041.

Note: A preliminary evaluation of MGB P/N 65351-11500, S/N A16-426, was conducted on 24 September 2007. See TSD&D-07-032 for details associated with that evaluation.

Evaluation Comments:

Prior to disassembly approximately 10 gallons of oil was drained from the sump thru a filter, with no chips or other significant debris detected. All chip detectors and lubrication jets were then removed and inspected for debris. No significant debris was found.

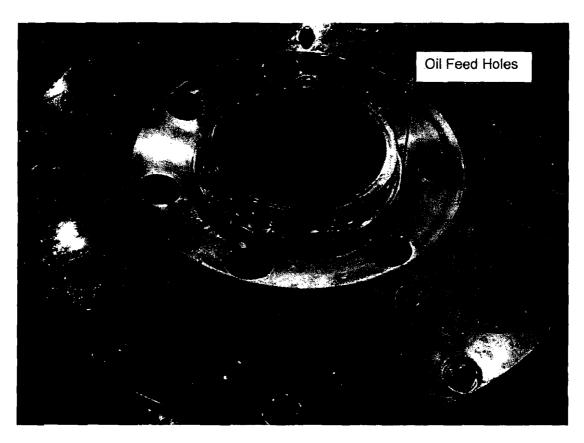
Both RH & LH Input Bevel Gear Assemblies were removed and visually inspected showing no damage or other indications of abnormal wear. Each unit rotated freely prior to and after removal. Both the LH and RH bevel pinions showed no surface distress and had acceptable contact patterns.

The torque of the T.T.O. nut, P/N 65351-11552-101, was checked in the tightening direction and measured 600 ft-lbs. The required B/P torque value is 425-475 ft-lbs.

The torque of the Free Wheel Unit nut, P/N 65351-11157-101, was checked in the tightening direction and measured 800 ft-lbs. for the RH unit and 1000 ft-lbs for the LH unit. The required B/P torque value is 400-500 ft-lbs.

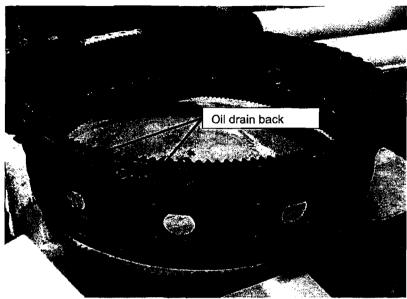
<u>Distribution Statement D</u>: Distribution authorized to the Department of Defense and DoD contractors only. The reports contain information on critical technologies and weapon systems operational tapabilities. Other requests shall be referred to WR-ALC/LUHJ.

The Second Stage Planetary Assembly (65351-11530-044) was removed and no visible damage was found. Both sides of the Lower Planetary Plate (65351-11537-102) were inspected using Fluorescent Penetrant Inspection (FPI), paying special attention to the oil feed holes. No cracks or other abnormalities were detected during the inspection process.



Second Stage Planetary Assembly, P/N 65351-11530-044

The Ring Gear (65351-11545-102) was removed and was found to have no abnormal wear and no notable anomalies. The gear was inspected using Magnetic Particle Inspection (MPI), paying special attention to the oil drain back holes. No cracks or other abnormalities were detected.



Ring Gear, P/N 65351-11545-102

The overall assessment was that gearbox exhibited normal wear with no notable anomalies.



January 3, 2008

LPM-H53-01-08-001

Warner Robins Air Logistics Center 226 Cochran Street Robins AFB, GA 31098

Attention:

LUHJE

Mr. Ray Goorah

Subject:

H-53 Intermediate Gearbox attachment hardware recommendations

During a recent safety investigation a discrepancy was found between the operator maintenance manuals and the Sikorsky Intermediate gearbox installation drawings. The NAVAIR, USAF and IAF field manuals call for the IGB attachment nuts, P/N SS5086-05, to be torqued to 200 inch-pounds. The Sikorsky installation drawing 65350-07100 specifies a torque value of 150/145 inch-pounds. The Sikorsky installation drawing 65350-07101 specifies a torque value of 145/140 inch-pounds. The torque-values were added to the drawings in the mid 1970's when the MS21042-5 nuts were replaced by SS5086-05 nuts.

It is recommended that the USAF conduct a review of the applicable field level maintenance manuals for the installation of the intermediate gearbox assembly (both 65357-07000 and 65357-07200 series). The torque value for the SS5086-05 attachment nuts shall be revised to reflect the corresponding blueprint torque value of 150/140 inch-pounds.

At the next overhaul of the intermediate gearbox assembly it is recommended to perform the following:

- 1) Check the center housing attachment studs for looseness per the applicable depot level maintenance manual.
- 2) During the fluorescent penetrant inspection of the intermediate gearbox center housing, pay special attention to the area adjacent to the attachment study for any crack indications

Please do not hesitate to contact me with any questions at (203) 386-3798.

Very Truly Yours,

SIKORSKY AIRCRAFT CORPORATION

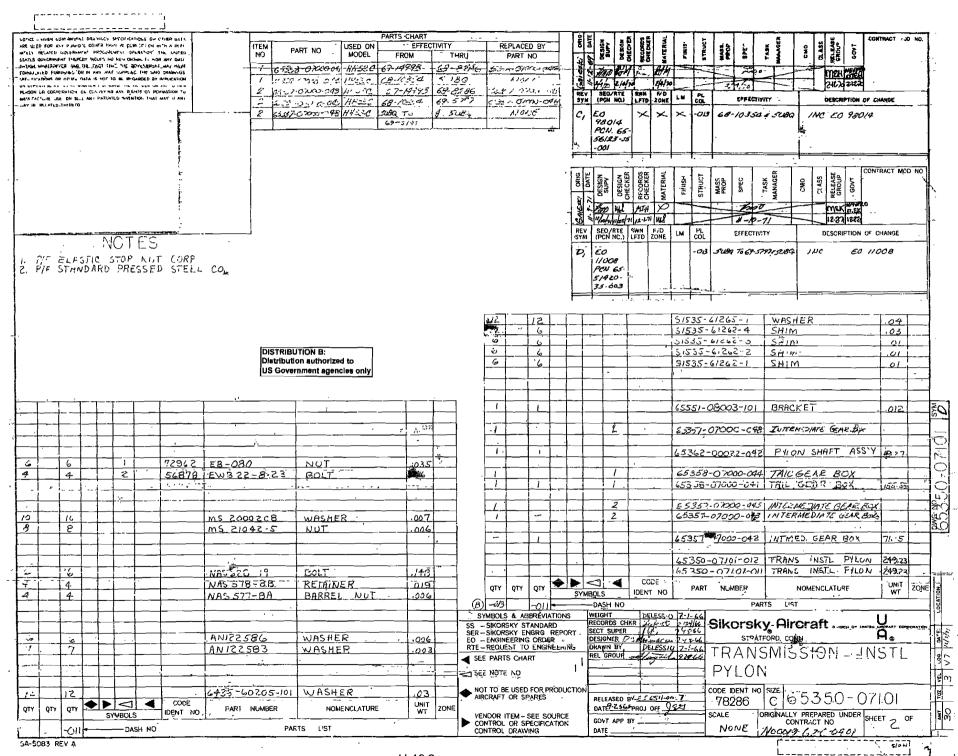
Mr. Joseph S. Fifer Jr.

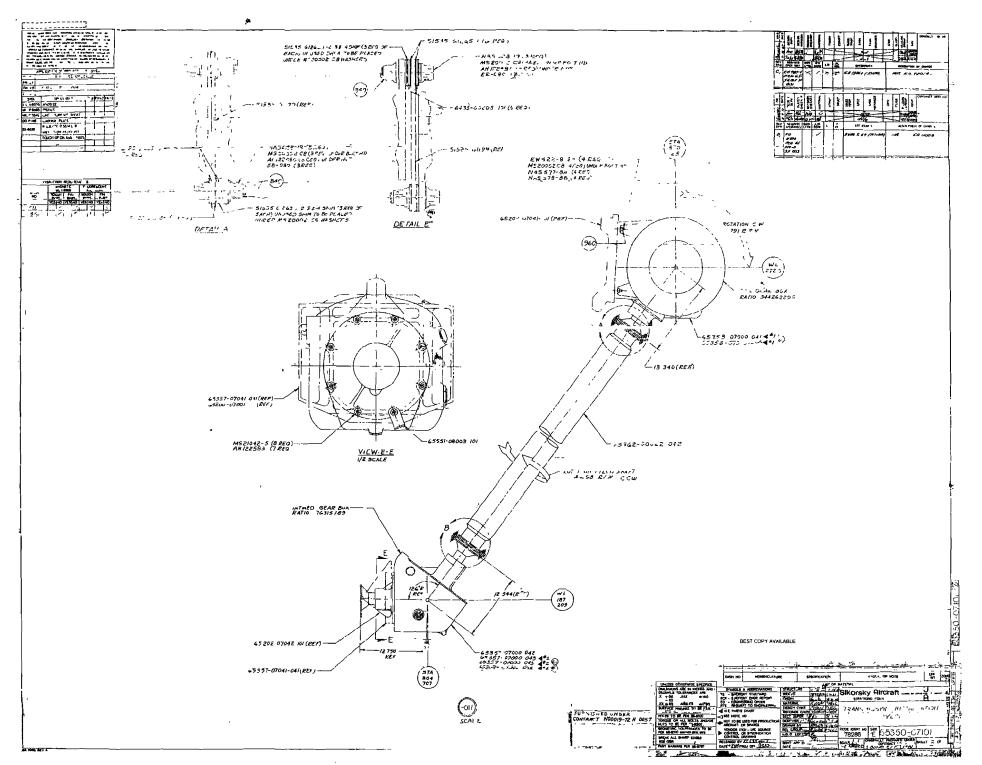
MH-53J/M Customer Service Manager

Worldwide Customer Service

ififer@sikorsky.com

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NOT MEASUREMENT SENSITIVE

MIL-HDBK-61A(SE) 7 February 2001

SUPERSEDING MIL-HDBK-61 30 SEPTEMBER 1997

MILITARY HANDBOOK

CONFIGURATION MANAGEMENT GUIDANCE



This handbook is for guidance only.

Do not cite this document as a requirement

AMSC N/A

AREA CMAN

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MIL-HDBK-61A

When the urgent or emergency priority is properly used, the contractor must be authorized to proceed with implementing the change as quickly as possible. Under these circumstances, it is often necessary to utilize a unilateral change order to the contract (or contracting officer letter) to provide official authorization to proceed. If the change order is to be used, a "not-to-exceed" price quotation (a "not-less-than" price for cost reduction ECPs) would be required to set a limitation on the price impact of the change activities to be accomplished. After the change order is issued, it is important to proceed as expeditiously as possible with the normal "definitization" process to minimize the risk of related price increase (or to maximize the related savings) resulting from the change.

VECPs are subject to essentially the same CCB process as other ECPs. Under the FAR clause, the Government is entitled to reimbursement of expenses incurred in processing an approved VECP before any cost savings are shared out to the contractor. Therefore, the tasking activity must develop auditable government cost information so that the complete monetary impact of the VECP can be evaluated. Any delays in VECP processing will typically reduce the savings benefit.

b. <u>Dispositioning Class II ECPs.</u> Unless otherwise specified by contract (e.g., as part of the Single Process Initiative), the government administrative contracting officer or plant representative serves as the dispositioning authority for Class II ECPs.. The default action required on Class II changes is concurrence/non-concurrence in classification only, unless the contract requires approval/disapproval. Government concurrence in Class II ECP classification normally allows the contractor to incorporate the change in the applicable CI and update its configuration documentation without any further government action or authorization being required. A non-concurrence in classification will normally result in the Class II ECP being canceled or reclassified to a Class I ECP.

The government should require approval/disapproval of class II ECPS only when the Government is the CDCA for the original drawings, or data files, and compliance with the specific detailed design is a requirement of the contract. If there is a government ACO or plant representative available, the Government tasking activity may elect to have the ACO or representative review the proposed class II changes for concurrence in classification before they are submitted to the government tasking/procuring activity (that is the CDCA) for approval [Details: Activity Guide: Table 6-7]

- 6.2.1.5 <u>Implementing Class I ECPs</u>. When ECPs are approved, change implementation to a CI being produced under contract is usually a straightforward contractual incorporation of the ECP as approved by the government CCB. CCB approval action is not to be considered authority for the contractor or tasking activity to proceed with the change.
 - A CCB directive must be prepared, published and distributed. The CCB directive is identified by the CCB identifier and the change identifier. The date of the CCB directive and disposition are recorded.
 Distribution should be limited to those parties required to take action to implement the change
 - If implementation of the approved change is the responsibility of the contractor under the terms of a
 contract, the CCB approval action directs the procurement contracting officer to initiate instructions to the
 contractor
 - If Contractor-initiated change proposals are involved, the receipt of a formal contract change for example, Standard Form 30, "Amendment of Solicitation/Modification of contract" or PCO letter (pending receipt of an amendment) shall constitute sole authority for the contractor to proceed.
 - If the initiator is government activity acting in the capacity of a contractor, the receipt of the directive/order (including funding authorizations) shall constitute sole authority to proceed with the change.

Change implementation to a CI in the inventory or operational forces will normally require the coordination of additional requirements of an implementing CCB directive (or tasking order).

- Necessary instructions and funding authorizations must be issued for the scheduled implementation of the change
- Change accomplishment reporting is directed. [Details: Activity Guide: Table 6-8]

The incorporation of approved changes should be planned so that optimum acquisition, production, tests, evaluation and operational advantages can be derived from the modified configuration. The change is effectively coordinated to

MEMBER: 1 FILE NUMBER :: 6 ADD FILE NUMBER :: 6 :: 772298 ACCESSION NUMBER DATE OF LAST EDIT :: 2008-01-23 SUBJECT :: Generator assy requires functionality check for proper operation at the request of the SIB investigation DATE INPUT TO INFOCEN :: 2007-10-01 ORIGINATOR ADDRESS :: HQ AFSOC/A4MYH ORIGINATOR INSTALLATION :: Hurlburt Field AFB, Fl., 32544 ORIG NAME/PHONE NR/DT SUB :: TSqt Andrew D. Jones, Com 850-884-7659, DSN 579-7659 AF CRITICAL ITEM (Y/N) :: N ORIGINATING POINT :: 1 SOMOS/MQP ORG PT NAME/PHONE NR/DT VER:: TSqt Kenneth Dockery, Com 850-884-7571, DSN 579-7571 Orig Pt Office Email Addr :: 1somxg.dr@hurlburt.af.mil REPORT CATEGORY (1 OR 2) :: 1 CATEGORY PRIORITY :: 1A OPERATIONAL IMPACT :: CRASH INVESTIGATION QA1 OR QAKA/QAKE REPORT :: OA1 REPORT CONTROL NUMBER :: FB4417070365 MISHAP/HAP CONTROL NUMBER :: 110524 MISHAP CLASS :: A :: 6115-00-292-4779 BZ NATIONAL STOCK NUMBER NOMENCLATURE :: GENERATOR, ALTERNATI DATE DEFICIENCY DISCOVERED :: 2007-09-07 MANUFACTURER SOURCE :: HONEYWELL INTERNATIONAL INC :: WRALC OVERHAUL/REPAIR SOURCE MANUFACTURER (CAGE) CODE :: 64547 OHAUL/REPAIR SRC CAGE CODE :: UNK MAINTENANCE TYPE :: C MANUFACTURERS PART NUMBER :: 28B58-57A REQUISITION NUMBER :: FB4417 ITEM NEW OR REPAIRED :: R END ITEM MDS :: MH053 :: 69-5794 END ITEM SERIAL NUMBER UNIT COST :: 18092 ITEM UNDER WARRANTY (Y/N/U):: N DETAILS/PROBLEM SUMMARY :: Circumstances Prior to Difficulty: Component requires evaluation for functionality per the request of the SIB investigators Requested exhibit analysis: Analyze/investigate root cause. Requested PQDR Exhibit Action: Repair MAJCOM/ACTIVITY CODE :: 0V COUNTRY :: USA SOURCE OF SUPPLY :: FLZ EXBT SUB HOLDING STATUS

:: A30

HOLDING ACTIVITY ADDRESS :: AFSOC SIB/afsoc.sib2@hurlburt.af.mil SAFETY OFFICER/PHONE NO :: Maj David Nicholson, Com 850-884-2081,

579-2081

SAFETY OFFICER EMAIL :: david.nicholson@hurlburt.af.mil

QA/EQUIP SPECIALIST/PHON NO:: MARK KUTAY, DSN 497-6953 QA/EQUIP SPEC/EMAIL ADDRESS:: mark.kutay@robins.af.mil

QA/EQUIP SPEC OFFICE SYMBOL:: 573 ACSS/GFLCC

QA/EQUIP SPECIALIST CODE :: H

DR/MIP STATUS :: OPEN

MIP PRIORITY :: U

TYPE DEFICIENCY :: MDR

SUBMITTED DR TYPE :: PODR

LAST UPDATE :: 2008-01-23
NEXT UPDATE DUE :: 2008-03-23

EXBT RQRD/RQSTD/HOLD Y/N/H :: Y

DTE EXBT INSTRUCTS PROVIDED:: 2007-10-16

EXBT SHIP-TO ADDR/INSTRUCTS:: (2007-10-16) N3096A, Fleet Readiness

Center

Southwest Customer Service, Bld. 341 San

Diego,

CA 92135 Attn. S. Manganelli

PROJ ENGINEER/PHONE/OFFICE :: JIM SAWINSKI, DSN 497-6950,

JAMES.SAWINSKI

ROBINS.AF.MIL

DATE RECEIVED AT SPOCO :: 2007-10-02

TREND ANALYSIS INDICATOR :: Total=4 Open=2 Closed=2 Last6=2 Last12=2

Last24=2 MDS=2 MH053;1 MH053J;1 MH053M;;

RO21=12 CAT1=2

Originator Email Address :: andrew.jones@hurlburt.af.mil
Originator ID :: kenneth.dockery@hurlburt.af.mil

MANUFACTURER ANALYSIS INDIC:: Total=220 Open=12 Closed=208 Last6=15

Last12=26

Last24=67 RO21=309 CAT1=13

OVERHAULER ANALYSIS INDIC :: Total=323 Open=51 Closed=272 Last6=120

Last12=172 Last24=230 RO21=114 CAT1=16

ACTION SUMMARY ::

(2008-01-23) Per Engineer Steve Manganelli at North Island: Subject generators were functionally tested on 17 Jan 08 to salient acceptance criteria listed in NAVAIR Manual 03-5AS-31, that normally applied to post-overhauled units at FRC-SW. Tests included no-load excitation current and voltage balance, PMG no-load voltage, PMG full load voltage, output full load excitation current and output voltage balance, 150% load, and overspeed (non-excited). Both generators were run simultaneously on a "feedback" test stand, each as UUT and slave. Both generators performed within acceptance limits. Prior to run, the cooling air "hats" were removed for FOD inspection with none noted. (2007-11-09) Request for TCN submitted 6 Nov 07; awaiting that info from AFSOC

to track property. No 'Q' assets are showing in Legacy systems for identified

NSN.

(2007-10-16) Shipping instructions received from North Island; i660 has been updated.

(2007-10-11) Report was transferred to North Island in error. Per telecon with

FSC at Cherry Point, this report will be closed administratively in NAMDRP.

Item should be investigated by Air Force engineering team since it is related

to a mishap. If items are slated for repair at a later date, NAVAIR will get

involved at that time.

(2007-10-05) Report will be transferred to North Island for investigation and

resolution. North Island POC will also be contacted by email to ensure that

disposition instructions are received in a timely fashion. (2007-10-02) Assigned to ES Mark Kutay, with engineering support provided by Jim Sawinski.

--- Critical/Major/Minor Defects ----

Location Assigned	Order	MDS	Tail#	Scheduled to Retire Date/Timeline	Additional Notes
Hurlburt Field	18	MH-53M	73-1649	Retire no later then Oct 08	Selected for PEMA museum input
Hurlburt Field	17	MH-53M	68-10924	Retire no later then Oct 08	
Hurlburt Field	16	MH-53M	73-1652	Retire no later then Oct 08	
Hurlburt Field	15	MH-53M	70-1631	Retire no later then Oct 08	
Hurlburt Field	14	MH-53M	68-10369	Retire no later then Oct 08	Selected for Hill AFB museum input
Hurlburt Field	13	MH-53M	73-1648	Retire no later then Oct 08	
Hurlburt Field	12	MH-53M	68-10357	March/April timeframe	Selected for Wright Pat AFB museum input
Hurlburt Field	11	MH-53M	69-5785	Retire no later then Oct 08	
Hurlburt Field	- 10	MH-53M	70-1626	Retire no later then Oct 08	Selected for WR-ALC museum input
Hurlburt Field	9	MH-53M	70-1629	Retire no later then Oct 08	
Hurlburt Field	8	MH-53M	68-8284	Retire no later then Oct 08	Added as a BAI aircraft
Hurlburt Field	7	MH-53M	69-5790	Retire no later then Oct 08	Added as a BAI aircraft
Hurlburt Field	6	MH-53M	67-14995	Retire no later then Oct 08	aprilonity SIVAVE perione garrent off
Mildenhall	5	MH-53M	67-14994	Retires no later then Oct 08	Transferred to HFLD from RAFM
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Hurlburt Field	4	MH-53M	69-5794	Retire no later then Oct 07	r 📑 🦥 Tro Pentra Fendino SIB/AIB Disposition
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Updated 28 Jan 08

Anthony, Frizi S TSgt MIL USAF AFSOC/CCX

From:

Halvorson, David L MSgt MIL USAF 1SOHMXS/MXAG [David.Halvorson@hurlburt.af.mil]

Sent:

Sunday, October 28, 2007 4:29 PM

To:

Stohler, Michael S Maj MIL USAF AFSOC/A8PP; Whitfield, Bernabe F Capt MIL USAF

1SOHMXS/MXA

Subject:

RE: 5794 AMARC

Sir,

It was suppose to depart with 356 and 358 which went out on 2 Oct for induction on 5 Oct.

V/r

MSgt Halvorson

----Original Message----

From: Stohler, Michael S Maj MIL USAF AFSOC/A8PP

Sent: Sunday, October 28, 2007 4:19 PM

To: Whitfield, Bernabe F Capt MIL USAF 1SOHMXS/MXA Cc: Halvorson, David L MSgt MIL USAF 1SOHMXS/MXAG

Subject: 5794 AMARC

Bernie, what was 5794's exact input date to AMARC?

Thanks,

Maj. Stohler

TAB AA

FLIGHT DOCUMENTS

MISSION CONTROL DATA.

AA-2

	TIME	WOW	Lat System	Long System	Groundtrack System	Groundspeed_System	All/tude System	THDG 5vs
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	03:12:42	ű	30,4025	-86.7025	206	118	920	
	03:12:47	9	30.4		216	117		
	03:12:52	Ü		-86,70616667	226	115	828	
					237	112	964	
	03:12:57 03:13:02	0		-86.71116667	249	110		
					260	110	4	
	03:13:07	0		-86.717	260 260	112		
	03:13:12	0		-86,72	259	114		
	03:13:17		30.39366667		259 259	150		
	03:13:22		30.39316667	-86.723	259 259	117 117		
	03:13:27		30,39266667	-86.726	259	***		
	03:13:37			-86.72915667	259 259	117		
	03:13:37			-86.73233333	479 260	117		
	03:13:42			-86,73533333	260 260	116		
	03:13:47	0			261	115		
5:19:43	03:13:52	0	30.39018687	-86.7415	103	1 8.3	%F 4.4° 46	

						_	
4-* \$6-48	03:13:57	ð	30.38983333	-86.7445	262	115	956
	03:14:02	Ó	30,3895	-86.7475	262	113	950
	03:14:07	õ		-86.7605	263	117	958
				-88,78,25	264	108	976
	03:14:12	0				107	980
5:20:08	(13:14:17	٥		-86,75633333	260	· · · · · · · · · · · · · · · · · · ·	956
5:20:13	03:14:22	0		-86,75933333	266	109.	
5-20-18	03:14:27	Ó.	30.38833333	-86,76216667	285	111	928
	03:14:32	ō		-85,76516667	264	113:	
				-86.766333339	264	113	872
	03:14:37	Ő		~00.F0000000	284	114	552
	03:14:42	0		-86,77133333		114	832
5:20:38	03:14:47	ä	30.38716867	-86.77433333	263		
5:20:43	03:14:52	9	30,36683333	-86:77733333	263	114	820
-, .,	03:14:57	0	30,3865	-56,7605	265	114	872
	03:15:02	ő	30.38633333	-86.7835°	265	113	804
				-86.7865	266	112	504
	03:15:07	9	30.38616667			109	812
5:21:03	03:15:12	0	30.386	-86.7395	260		828
5:21:08	03:15:17	0		-86.79233333	267	107	
5/21/13	03:15:22	Ď	30,3856667	-36,79516667	267	106	836
	03:15:27	0	30,3855	-86.798	.264	106	836
				-89,80083333	263	107	840
	Q3:15:32	0			202	107	\$52
	03:15:37	0		-86.80383333		107	860
	03:15:42	0		-86.80666667	262		872
5:21:38	03:15:47	0	30.38416667	~86.8095	263	107	
	03:15:52	0	30.38383333	-86.81233333	264	106	663
	C3:15:57	â		-86:81516667	264	106	872
	03:16:02	ä	30.38333333	-86.818	2 65	105	880
				-86.62063333	265	104	888
	03:16:07	G				105	892
	03:16:12	۵	30.3 5283 333	-86.8235	264		888
5:22:08	03:16:17	0		-86.62633333	264	106	
	03:16:22	0	30.38233333	-86.8Z916667	265	106	876
	C3:16:27	0	30,38216667	-86.832	.266	106	006
	03:16:32	o o		-66.83483333	202	102	852
				-86.63716667	317	162	832
	03:16:37	0			357	105	783
5:22:33	03:16:42	0		-86.83833333			772
5.22.33	03:16:47	O	30,38783333	-86.83766667	33	105	
5.22.43	03:16:52	ø	30.3895	-86.83566667	55	188	780
	03:16:57	Ó		-86.83316657	.69	108	804
		ő		-86.83033333	88	108	836
	03:17:02				r io	105	892.
	03:17:07	9	30.39083333		118	108	960
	03.17.12	Ò	44	-86,82483333			1032
5:23:08	03:17:17	٥		-66.82233333	119	107	
5:23:13	03:17:22	0	30.3875	-86.81963333	118	108	1100
	03:17:27	ø	an 38033333	-86.81716667	116	109	1144
			30.38518687	-86.8145	111	111	1188
	03:17:32	Ď.		-86.81166667	ioo	112	1236
5:23:28	03:17:37	0				i14	1208
	03:17:42		30.38433333		91		าลิบซ์
5:23:38	03:17:47	.0	30.38433333	-86.80566667	යිරි	114	
	03:17:52	0	30,38433333	-86.8025	96	113	1348
**	03:17:57	Ó	30.394	-88,7995	94	113	1388
	3 1		30.384	-88.7965	87	112	1380
	03:18:02	ű			84	112	1368
	03:18:07	Q	30.38416667	-85,7935		* ' '** 111	13 5 8
5:24:03	03:18:12	Q	30.3845	-86.790s	84		
5:24:08	03:19:17	0	30.38483333	-85.7875	82	111	1340
	03:18:22	0	20 38516667	-26.78466667	82	111	1316
	03:18:27	ō		-86.78166567	82	111	1300
				-86.77 8 68667	ខ ែ	110	1292
	03:18:32	0				109	1284
5:24:28	03:13:37	0		-86,77583333	82		1276
5:24:33	03:48:42	Q	30.3866667	-86.77283333	81	109	
	03:18:47	ð	30.387	-86.77	81	108	1256
	03:18:52	ő	30.3475	-86.76716667	80	107	1240
_				-86.76433333	80	105	1228
	03:18;57	0			81	104	
	03:19:02					103	
5:24:58	03:19:07	0			80		
5:25:03	03:19:12	0	30.38916667	-88.75615567	80	102	
	03:19:17	0	30.3895	-86.7535	81	101	1120
		ő		-86.75083333	83	190	1096
3.2503	03:19:22	ù.i	المُرْجِينِ فِي الْمُرْجِينِ وَيَدِينِهِمْ فِي الْمُرْجِينِ وَيَدِينِهِمْ فِي الْمُرْجِينِ وَيَعْدُ	الباد المناه المدادية المهافية البادية المراجعة			

5:25:18	03:19:27	0	30.39	-86,74816667	85	100	1064
			30.39016657	-86.7455	85	100	1028
1	03:19:32		y				
5:25:28	03:19:37	0	30.3905	-86.74268667	84	100	1000
5:25:33	03:19:42	O	30,39066667	-86.74	84	99	976
K-25-38	03:19:47	a	30.391	-86.7375	84	98	952
				-86.73483333	84	97	932
44 14	03:19:52						
5:25:48	03:19:57	Ü	30.3915	-86.73216667	84	97	912
5/25:53	03:20:02	0	30.39166667	-86.72986667	84	96	892
1 '	03:20:07			-86.72716667	84	95	884
5:28:03	03:20:12	0	30,39216667	-88.7245	64	94	864
5:26:08	03:20:17	0	30.39233333	-86.722	85	,93	844
B-28-53	03:20:22	0	30.3925	-86.7195	65	92	820
1					85	92	612
	03:20:27			-86.71716667			
5:26:23	03:20:32	Q	30.39283333	-86.71466667	84	91	808
50698	03:20:37	ű	30.39316667	-86,71233333	83	90	812
	03:20:42			-86.70983333	83	90	816
					**		
5:26:38	03:20:47	0	30-39366667	-86.7075	82	90	828
5:26:43	03:20:52	٥	30.394	-86.708	81	50	832
	63:20:57			-86,70266667	30	91	836
1							
	03:21:02	,U		-86,70016667	79	91	832
5.26.58	03:21:07	Ü	30.39516667	-86.69783333	78	91	832
62703	03:21:12	Ð	30.3955	-86.6955	77	9*	824
1					72	93	780
	03:21:17	Ö		-86.69316667			
5:27:13	03:21:22	Ü	30.397	-86.69083333	61	:95	692
5:27:18	03:21:27	Ω	30.39816867	-86.68866667	49	97	608
	03:21:32			-86.68683333	40	9.8	536
					,		
5:27:28	03:21:37	0	30.40166667	-86.68533333	28	98	475
5:27:33	03/21/42	0	30.40383333	-86.68 433 333	15	96	432
	03/21/47	0	30 406	-86,68383333	7	94	392
					4	92	364
	03:21:52			-86.68366667			
5:27:48	03:21:57	0	30.41016667	-86.6835	2	85	344
5:27:53	03:22:02	0	30.41216667	-86,6835	358	78	320
5.77.54	03:22:07	Ö	30.41383333	-96 68366667	358	70	292
					358	43	264
	03:22:12	0		-86.68366657			
5:28:08	03:22:17			-86.68383333	365	56	240
5:28:13	03-22-22	0	30.41816667	-86,68383333	356	51	220
	03:22:27	0	30,41916667	-86.684	358	41	200
						33	180
5:28:23	03:22:32	0	30.42	-86.684	352		
5:28:28	03:22:37	0	30.42083333	86,68416667	. 355	27	156
6.28.33	03:22:42	Ü	30 42 13 33 33	-86,68416667	353	21	132
	03:22:47		30.42163333		357	19	116
						·	
5:28:43	03:22:52	0	30.42216667	~80,004,33333	35 3	16	108
5:28:48	03:22:57	O	30.42266667	-86.68433333	356	13	85
4.94.53	03:23:02	0	20 40 28 2333	-88.68433333	356	8	92
				i i	358	6	72
	03:23:07	0		-86.68433333			
5,29:03	03:23:12	0	30.42316667	-85.6845	356	3	56
5:29:08	03:23:17	٥	30.42316667	-86.6845	357	2	44
- menone a sound		-		0			
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	03:24:14		30.42316667	-86.6845	358	•	
6:30:10	03:24:19	0	30,42333333	-86.6845	351	10	64
	03:24:24		30.42366667	-86.8845	356	25	72
	03:24:29				358	40	92
		ā	30.4245	-86.6845			
5:30:25	03;24:34	0	30,4255	-86.68466667	362	56	120
5:30:30	03:24:39	0	30.427	-86,685	348	72	144
	03:24:44		30.42883333		351	83	164
					354	92	192
	03.24:49		30.43083333		·		
5:30:45	03:24:54	Q	30.433	-86.68683333	O	95	240
5:30:50	03:24:59	Ω	30.43516667	-86.6855	₹₿.	92	316
	03.25.04	ã		-56.68433333	44	89	380
						87	416
	03:25:09	ā		-86.68233333	77		
5:31:05	03:25:14	٥	30.438	-86.63	112	89	428
	03:25:19	٥	30.43666667	86.6785	140	91	448
	03:25:24	Ö		-86.67716867	154	93	496
	03:25:29			-86,67616667	184	96	556
5:31:25	03:25:34	O	30.43066667	-86.67566667	173	98	608
	03:25:39		30.42833333	-86,6755	† 79	101	644
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8:31:35 03:25:44	o 30.426 -8	6,6755 1 3 0	104	672
5:31:40 03:25:49	0 30.4235 -86.675		108	696
	0 30.42083333 -86.675	6. A. C.	113	704
5:31:45 03:25:54		and was also as a	118	704
5:31:50 09:25:59	0 30.41816667 -86.675		119	700
5:31:55 03:26:04	0 30.4155 -86.675			696
5:32:00 03:26:09	p 30,41266667 -86,575		123	
5:32:05 03:26:14	0 30.40983333 -85.675	182333	120	688
5;32:10 03:26:19	0 30.40716667 -85.576		118	620
5.32:15 03:26:24		8,6775 219	108	572
		4.18.1.4	100	520
5:32:20 03:26:29	0 30,40333333 -86,679		92	468
5:32,25 03:26:34	0 30.4035 86.682			406
5:32:30 03:26:39	n 30.405 -86.683		88	
5:32:35 03:26:44	0.30.40716667 -4	26,684	89	384
5:32:40 03:26:49	0 30,40916667 -86,683	183333 358	90	338
5:32:45 03:28:54		86.684 354	äï	384
		an service .	àż	388
5.32:50 03:20:59			70	376
5:32:55 08:27:04	0 30.415 -86.684			340
5:33:00 03:27:09	0 30,4165 -86,684			296
5 33 05 03 27:14	0 30,41783333 -8	8.6845 357	50	
5:33:10 03:27:19	0 30.41883333 -86,684	1 8 6667 · 356	44	252
5:33:15 03:27:24	0 30,41983333 -86,684		39	208
	0 30,42066667 -86,684		33	172
5:30:20 03:27:29			29	144
5:33:26 03:27:34	0 30.4215 -86.684			120 -
5:33:30 03:27:39	0 30,422 -86,684		25	100 -
5:33:35 03:27:44	0 30,42255557 -	86,685 355	18	
5:33:40 03:27:49	0 30,42263333	86,685 355	11	58 <u> </u>
5:33:45 03:27:54		86.685 353	б	34 -
	3. 12 3.1	96.685 352	5	68
5,33,50 Q3,27,59		an arm who is	ë	48
5.33.55 03:28:04	0 30/42333333 -4	and the same of the	~	
		0	: 25"	52
5:35:25 03:29:34	0 30.42333333 -4	85,565 354	2	
5:35:30 03:29:39	0 30.42333333 -4	86.695 358	1	52
5:35:35 03:29:44		86.685	3	60
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	Mar and a survey of the control of t	96.885 355	1	72
5:35:45 03:29:54	All the state of t	W AC 1995 13 15	4	64
5:35:50 00:29:59			*	50
5:35:65 03:30:04		352		64
5/36:00 03:30:09	0 30,42316667	86,685 352	4	
5:38:05 03:30:14	0 30.42316667 -4	86.685	D .	56
5:36:10 03:30:19		86.585 355	0 -	56
		56,685 355	Ð	60
5:36:15 03:30:24			. 2	GD .
5:36:20 03:30:29	At . M. M. C. M. At		8	64
5:36:25 03:30:34	s var.	86.885 352		68
5:36:30 Q3:3Q:39	0 30,42366667 -4	88,685	17	
5:36:35 03:30:44	0 30 42416667	86,885 358	24	68
5:36:40 03:30:49		86,586 357	38	84
5:36:45 03:30:54		98.885 359	51	96.
		Section 1 to 1	58	140
5:36:50 03:30:59			71	164
5:36:55 03:31:04	0 30.42866667 -86.885	'a atau	85	152
5:37:00 03:31:09	0 30,4305 -86,685			
5:37:05 03:31:14	g 30.4325 -86.685	13,133 356 356	94	160
5:37:10 03:31:19		6.6855	98,	212
		BB 685 21	. 100	304
5:37:15 03:31:24	4.07 1.04 0	6.6835 44	% 01	396
5:37:20 03:31:29		· · · · · · · · · · · · · · · · · · ·	101	480
5:37:25 03:31:34	0 30.44033333 -86.681			532
5:37:30 03:31:39	0 30.440 86 667 -8	6.6785 94	104	
5:37:35 00:31:44	0 30.44 -86.575	i83333 121	107	560
5:37:40 03:31:49	0 30,43816867 -86,673		109	592.
			112	620
5:37:45 03:31:54		• • • • • • • • • • • • • • • • • • • •	115	632
5:37:50 03:31:59	0 30.43316667 -86.572			648
5.37:55 03:32:04		66.673 183	118	
5:28:00 03:32:09	0 30.42766667 -86.673	316667 183	120	664
5:38:05 03:32:14	0 30.42483333 -86.673		119	704
	0 30,422 -86,673		118.	736
5:38:10 03:32:19		6.6735	118	752
5:38:15 03:32:24			118	756
5:38:20 03:32:29	0 30,4185 -88,673	182	: 2·2	
	* *			

5:38:25 03:32:34	0 30.41383333	-86.6 7 383333	182	116	764
5:38:30 03:32:39	0 30.41116667		181	117	764
5:38:35 03:32:44	0 30 40833333		181	115	772
April 10 to the total to the to	(2 m 3) (4 d 3 m 4 m 4)	- 10-14	180	114	768
5:38:40 03:32:49		-86.67383333			744
5:38:45 03:32:54		-86.67383333	179	113	
5:38:50 03:32:59		-86.67383333	180	; 12	724
5:38:55 03:33:04	0 30.39783333	-86,674	188	111	680
5:39:00 03:33:09	0 30.39533333	-88.67466687	204	107	644
5:39:05 03:33:14		-86.67633333	225	102	628
5:39:10 03:32:19		-86.6785	25 0	150	596
					564
5:39:15 03: 3 3:24	0 30/392		283	101	
5:39:20 03:33:28	0 30.39316667	-86 6835	324	100	524
5:39:25 03:33:34	0 30.39533333	-86.68416667	0	100	476
5:39:30 03:33:39	0 30.39766667	-86.684	7	95	508
5:39:35 03:33:44	0 30.39983333		3	91	548
5.39:40 03:33:49	0 30.40183333		1	88	544
		· ·	; 1	82	532
5:39:45 03:33:54	0 30,40383333				
5:39:50 03:33:59	0 30 40566667		0	75	516
5,39,55 03:34:04	0 30,40733333		358	66	492
5:40:00 03:34:09	0 30.40883333	-88,68383333	359	58	480
5:40:05 03:34:14	0 30.41016667	-86.68383333	359	52	484
5:40:10 03:34:19		-86 68383333	D	52	496
		-86.68383333	358	52	508
5:40:15 03:34:24				53	524
5:40:20 03:34:29	0 30.41366667	-86.684	354	and the second s	
5:40:25 00:34:34	0 30.415	-86 684	352	52	552
5:40:30 03:34:39	0 30,41616667	-86,68433333	354	50	556
5:40:35 03:34:44	0 30.41733333	-86.68433333	357	48	560
5:40:40 03:34:49	0 30.418333333	-86,6845	9	46	652
5:40:45 03:34:54	0 30.41933333	-86.8845	o	40	536
5:40:50 D3:34:59	w w.v	-86.68433333	2	32	464
				23	392
5:40:55 03:35:04	0 30.42083333		0		
5:41:00 03:35:09	0 30,42133333	-86.68433333	363	19	328
5.41.05 03:35:14	0 30.42183333	~86.6845°	351	17	252
5:41:10 03:35:19	0 30.42218667	-86.6845	349	15	196
5:41:15 03:35:24		86.68465667	350	13	160
5.41:20 03:35:29		-86.68483333	351	10	136
			352	8	108
5:41:25 03:35:34	0 30.423	-80.685			
5:41:30 03:35:39	0 30.42316667	-86.685	352	6	92
5.41:35 03:35:44	0 30.42316667	-86.685	352	4	64
		O			
5,43:20 03:37:29	0 30.42933333	-86,685	352	3	56
5:43:25 03:37:34	0 30.42333333	-86.685	356	1	108
5:43:30 03:37:39	0 30.4235	-86.685	356	7	140
			354	14	158
5:43:35 03:37:44	0 30.42386867	-86.685			
5:43:40 03:37:49	0 30.424	-86.685	1	14	172
5:43:45 03:37:54	0 30.4245	~86.685	356	25	184
5:43:50 03:37:59	0 30.42516667	-86 .685	350	40	204
5:43:55 03:38:04	0 30.426333333	-86.68516667	357	57	236
5 44 00 03 38 09	0 30.42783333		356	74	264
			356	89	278
5:44:05 03:38:14	0 30 42983333	-86.6855			300
5:44:10 03:36:19		-86.6856667	355	101	
5:44:15 03:38:24	D 50.43433333	-86.68583333	358	108	316
5:44:20 03:38:29	0 30.437	-86 68566657	10	105	360
5.44:25 03.38:34	0 3043933333	86.68483333	23	106	412
5:44:30 03:38:39	0 30.44116667	-86.683	49	105	440
		-86,68066657	68	106	470
5:44:35 03:38:44					552
5:44:40 03:38:49	0 30.44333333	-86.678	74	104	
5:44:45 03:38:54		-86.67516667	79	105	628
5:44:50 03:38:59	0 30,44416667	-86.6725	85	107	680
5:44:55 03:39:04	0.30,44433333	-86.6695	91	110	720
5:45:00 03:39:09	0 30.444	-86.6665	107	112	752
		-88.66383333	124	112	778
5:45:05 03:39:14			140	114	792
5:45:10 03:39:19		-86.66166667			
5:45:15 03:39:24	0 30.43883333	-86,66	156	115	800
5:45:20 03:39:29	0 30.43616667	-80.65916867	169	116	804
5:45:25 03:39:34	0 30.4935	-86 ,65883333	178	118	798
		· ·			

5:45:30	03:39:39	a	30.43083333	-86,65886567	781	119	788
	03:39:44	0		-86.65883333	183	119	788
	03:39:49		30.42516667	-86.659	184	119	800
				-86.65916667	184	120	798
	03:39:54			-56.6505	184	121	788
	03:39:59		30,41966667		185	124	764
	03:40:04		30.41668667			125	738
5;46:00	03:40:09	0	30,41383333	-86,36	184		720
5:46:05	03:40:14	0	30,411	-88,68016667	183	126	
5/48/10	03:40:19	0	30.408	-86,66033333	182	123	720
	03:40:24		30.40516667	-86.66033333	181	122	712
	03:40:29	ő	30.40233333	-86.6605	180	120	703
		. 0	30.3995	-86.6605	181	118	718
	03:40:34			-86.6805	182	118	728
	03:40:39		30.39883333		195	113	698
	03:40:44	0		-88,68083333			852
5:46:40	03:40:49	Q		-86.68216667	221	110	628
5:45:45	03:40:54	Û	30.3905	-88.66466667	255	108	
5:46:50	03:40:59	0	30,39066667	-86.6675	290	107	584
	03:41:04	O.	30.39183333	-88.67	309	112	512
	03:41:09			-86,57216687	317	118	448
		ð	30.39566687	-86.67433333	315	117	400
40.7	03.41:14			-86.6765	315	114	320
	03:41:19	Ö	30.3975		316	111	356
	03:4.1:24	0	30.3995	-80.67866667		102	356
5:47:20	03:41:29		30.40133333	-85,52066667	321		436
5:47:25	03:41:34	0	30.40316687	-86.862	333	69	
5:47:30	03:41:39	0	30,405	-86.66283333	346		488
	03:41:44	: 0	30,40683333	-88,68316667	351	70	50B
	03:41:49		30.40833333	-85,6835	356	63	512
	03:41:54		30.40988687	-86.6835	357	57	518
				-86,68366667	358	54	512
	03:41:59	0.			357	55	512
	03:42:04	Ö		-86.88358667	357	48	524.
	03:42:09	٥	10-11-	-86.68366667		47	532
	03:42:14	. 0	30,4145	-86.66383333	356		544
5:48:10	03:42:19	. 0	30.4155	-86.66383333	354	46-	
	03:42:24	Ö	30.41666667	-86.584	351	50	556
	03:42:29	g	30.41783333	-86.68433333	349	50	.580
	03:42:34	ã	30.419	-86.8845	350	46:	496
	03:42:39	ő		-86.68466667	29	36	424
			30.42066667	-36.6846	ā	29	356
	03:42:44	g			355.	25	288
	03,42:49		30,42133233	-88,58468667	352	24	220
5:48:45	03:42:54	0	30.42183533	-86.88466667		20	168
	03:42:59	()		-86,68482333	351		128
5:48:55	03:43:04	8-	30 42283333	-86,66483333	344	17	
5:49:00	03:43:09	0	30.42316667	-56.685	346	15	112
	03:43:14	Q	30.4235	-86,885	353	13	. 58
~	03:43:19		30,42383333	-86.685	351	13	64
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c: rc.#6	2500 X 4. 100	a	30.42433333	-86.685	351	14	58
	03:44:01			-86.68516667	358	31	92
	03:44:08	Đ			355	46	132
	03:44:11	Ď				50	196
5:50:07	03:44:16	Ü		-86.68533333	353	74	252
5:50:12	03:44:21	ø	30,4285	-86.6855	355		296
5:50:17	03:44:26	0	30.43033333	-86.68566667	357	66	
	03:44:31	Q	30.4325	-86.8855	4.4	33	352
	03:44:36	ã	30.4345	-88,68466667	33.	98	404
	03:44:41	ő		-86.68256667	58	102	456
		ű	30.43716667	-86,68018667	75	105	488
	03:44:46			-86.67733333	92	710	520
	03:44:51	Ō	30.4375		106	113	576
5:50:47	03:44:56	٥		-86.67432333		116	624
5:50:52	03:45:01	Q	30,436	-86.6715	117		688
5:50:57	03:45:06	0	30.43486667	-86 56883333	127	116	
	03:45:11	Ö	30.43283333	-86.6665	139	117	740
	03:45:16	٥	30.4305	-86.66456667	151	119	760
	03:45:21	ŏ	30,428	-85_6635	164	119	764
		ŏ	30 40545657	-86.66283333	174	120	750
	03:45:26			-66.66266667	177	120	783
	03:45:31	0	30.4225		180	120	792
5:51:27	03:45:36	O.	30.41965667	-86.6625	100	,29	e mil.

5:51:37 5:51:42 5:51:47 5:51:52 5:51:57	02:45:41 03:45:46						
5:51:37 5:51:42 5:51:47 5:51:52 5:51:57		(1)	30.41683333	-86.6625	182	120	784
5:51:42 5:51:47 5:51:52 5:51:57		ő		-86.66266667	183	120	780
5.51,47 5:51.52 5:51.57			30.41116667		\$82	121	776
5:51:52 5:51:57		0	30.4085	-86.683	181	121	760
5:51:57			70.00		180		760
		.,	30.40566567	-86.663		121	
55 88 AN 25 M	03:46:06	Ç	30,40283333	-86,663	179	121	752
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5:52:07	03:46:16	0	3D.39716667	-66.66 2833 33	181	118	764
	03:46:21	Ó		-86.86316867	198	114	780
	03.46.26	4.1	30.39233333		223	110	780
	· ·			-86.66716667	249	111	740
	03:46:31	_				· · · · · · · · · · · · · · · · · · ·	676
	03:46:38			-86.67016667	270	116	
5:52:32	03:46:41	0		-86,67316667	288	119	524
\$:52:37	03:46:46	0	30,392	-86,67616667	302	119	596
5:52:42	03:46:51	D	30.39365667	-86.67866667	315	117	572
	03:46:56	D	30.39583333	-86.68066667	327	111	648
.,	03:47:01	ő	•	-86.68183333	339	100	568
		-			347	92	592
	03:47:06	Ô		-96.68266667	** **	* * * *	
	03:47:11	Ü		-86.68315667	352	84	612
5:53:07	03:47:16	O	30.404	-86.68333333	• 357	79	604
5:53:12	03:47:21	0	30.40583333	-86.68333333	359	73	584
5:63:17	03:47:26	0	30.4075	-86.6835	358	64	548
	03:47:31		30.40883333	-86.6835	2	5ë	518
	03:47:36		30.41016667	-86 6835	9	52	508 -
				-86.6835	357	52	508 -
	03:47:41		3D.41133333	7		54 54	496
	03:47:46	0		-86.68366667	352		
w., w. a.,	03:47:51	0	30.41383333		348	55	512
	03:47:56	0	30.415	-86.684 16667	348	54	540
5:53:52	03:48:01	D	30.41616667	-86.6845	350	50	540
5:53:57	03:48:06	0	30.41733333	-86,68466667	357	44	492
	03:46:11	Ö		86.68466667	3	38	440
	03:48:16	ő	30.419	-86,6845	4	31	388
				-86.6845	· e	27	344
•	03:48:21	Õ				25	300
	03:48:26	.0		-86,6845	357		
5:54:22	03:48:31	0	30.421	-89.6845	355	25	264
5:54:27	03:48:36	Ü	30.4215	-86.68466667	354	21	228
5:54:32	93:48:41	0	30.42183333	-86.68468667	342	16	188
5-54-37	03:48:46	a	30.42233333	-86.68483333	349	14	160
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	03:48:56	Ö		-86.685	352	10	
		4.5		-86,685	351		3 (146
		er				76	104 88
5:54:52		0	30.423			8	88
5:54:57	03:49:06	0	30.42316667	-86.685	353	4	88 64
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	03:53:14	0	30.4225	-86,583	181	513	740
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5:59:30	02:53:39	0		-89.66306867	182	111	
	03.53:44	.0	30.407	-86,66383333	181	110	772
	03:53:49			-86.66383333	179	111	768
	03:53:54		30.40183333		179	112	766
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	03:54:09		30,39383333			112	732
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6:00:10	03:54:19		30.38865667	-86.6635	179	111	
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	03:54:29	. 0	30,38386667	-86.66333333	17.7	104	808
	03:54:34	0		-88.68316667	179	105	836
	03:54:39		30.37856667		186	111	808
				-86,68366667	193	118	772
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	03:54:49	Ð		-86,66466667		124	852
	03:54:54	Ø.	30,37083333		213		720
8:00:50	03:54:59	0		-86.66816667	227	117	748
6:00:55	03:55:04	0	30.367	-85.67066667	238	117	
	63:55:09	Ó	30.36583333	-86.6735	254	114	784
÷	03:55:14	O	30 36566667	-86.6765	278	114	804
	03:55:19	ä	20.36633333	-86.67933333	298	17.5	840
	03:55:24	.o		-86.68166957	319	11%	964
			30.37016667		338	113	872
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	03:55:39	Ü		-88.68416667		128	816
6:01:35	03:55:44	0.		-96,68383333	6		780
6:01:40	03:55:49	Ö	30.381	-86.6835	7	122	756
6:01:45	03:55:54	0		-86,68316667	, 5	121	
8:01:50	D3:55:59	Ü	30.38666687	-86,68283333	4	122	712
	03:50:04	Ö.	30:3896	-85,68266557	~*	120	672
	03:56:09		30.39216667		359	114	652
	03:50:14	ŏ		-88,68283333	353	110	824
	03:56:19		30.39733333		247	106	612
					345	102	60 5
	03:56:24	0		-85.68483333	344	100	576
	03:56:29	0				93	532
m	03:56:34	0	30.40416667	-86.6855	346	86	492
5:02:30	03:56:39	Û-	30.40616667	-86,686	349		452
5:02:35	03:56:44	0	30.40816667	-86.6865	349	82	
6:02:40	03:56:49	Ö	30.41	-85,68683333	350	76.	420
	03:56:54	ä	30.41166687	-86.68716667	352	58	388
	03:56:59		30,41316667	-88,6875	353	60	344
		ă	30,41433333		354	51	292
	03:57:04			-86.68769667	358	40	248
	03:57:09	0			0	30	208
	03:57:14	ū	20.41030335	-85.68765567		24	180
	03.57:19	0		-86,00766667	365	20	148
6:03:15	03:57:24	0		-85.68783333	352		120
8:03:20	03:57:29	0		-86.68783333	354	17	
6:03:25	03.57:34	٥	30.41816667	-86.68783333	353	12	100
	03:57:39	ō	30.4185	-86.688	3 5 0	8	92
	03:57:44	Õ	30.41868657	-86.568	355	3	76
	03:57:49		30.41866687	-88.668	355	1	64
			30.41866687	-86.688	351	2	52
	03:57:54	0			352	, î	55
	03:57:59		and the second second	-86.686 22 22	337	1	56
	03:58:04	0	30.41866667	-86.568		Q	46
	03:58:09	0	30.41883333	-36,689	315		52
6:04:05	03:58:14		30.41883333	-85,688	29B	0	34 56
	03:58:19	Q.	30,41883333	-86.580	278	1	
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6:04:20			30,41866667	-86.689	204	2	64
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6:04:30	03:58:39	ũ	30 41866667	-85,688	121	1	68
	03:58:44		30.41866867	-86,68	75	2	72
		.,		·			
	03:58:49		30.41886667	-86.688	31	3	72
6:04:45	03:58::54	0	30.41866667	-86.688	356	1	72
6.04:50	03:58:59	0	30.41866667	-86.688	354	4	64
	03:59:04	Ö	30.41866667	-86,688	355	1	56
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5:05:00	03:59:09	Đ	30.41883333	-86.686	349	3	A\$ 14
				Ø			
8:06:02	04:00:11	Ω	30.41683333	-86,686	352	3	52
	04:00:16		30.41916667	-86.686	356	19	64
6:06:12	04:00:21	٥		-86.68816667	356	42	76
6:06:17	04:00:26	0	30.421	86.68816667	350	65	80
6:06:22	04:00:31	G	30 42283333	-86.68833333	356	83	88
	04:00:36	0	30 42483333	-80.6885	356	93	120
					355	99	172
	04:00:41	0		-86 68866667			
6:06:37	04:00:46	0		-86.68883333	355	103	216
6:06:42	04:00:51	. 0	30.43183333	-86.689	356	104	244
9.00-47	04:00:56	ð		86.68933333	356	108	276
	04:01:01	Õ	30.43683333	-86.6895	356	105	328
	04:01:06	0		-86,68966667	357	104	408
6:07:02	04:01:11	0	30,44166667	-86.68983333	358	104	484
6:07:07	04:01:16	Û	30.444	-88.68983333	-357	108	568
	04:01:21	ő	30.4465	-86.69	357	107	652
						107	700
	04:01:26	Ō:		86.69016667	356		•
5:07:22	04:01:31	0	30.4515	-86.69 05	355	107	740
6:07:27	04:01:36	Q.	30.454	-86.69066667	355	106	760
8-07-32	04:01:41	Ö	30,4565	-86.691	354	104	764
				-86 89133333	353	103	764
	04:01:46	· ·					
	04:01:51	0		-86.69166667	353	103	772
8:07:47	04:01:56	0	30.46366667	-86.692	353	105	768
6.07:52	04:02:01	0	ap. 466	-86.69233333	350	107	784
	04:02:06	õ		-86.69216667	* *	107	798
						107	804
	04:02:11	0		86.69133333	26		
6:08:07	04:02:16	Ü	30,473	-86.66983333	40	108	812
6:08:12	04:02:21	0	30.47466667	-86.58768667	56	107	840
6/08/17	04:02:28	Ø	30.47583333	-86.68516667	69	107	864
				86.68233333	80	108	884
	04:02:31	9					904
	04:02:36	Ω	30.47666667	-86.6795	93	106	
6:08:32	04:02:41	0	30.47616667	-86.5765667	167	105	908
6:08:37	04:02:46	0	30.47533333	-86,674	120	106	892
	04:02:51	0	30 47383333	-86.67183333	132	107	888
	04:02:56			-86.66983333	143	108	888
		0				,	
5:08:52	04:03:01	Ö	30.469833333	-86.66816667	152	108	898
8:08:57	04:03:06	Ü	30.4675	-86.66716667	161	108	· 892
8:09:62	04:03:11	0	30.465	-86.666333333	168	108	896
	04:03:16			-66.66566667	168	108	892
and the second of							988
	04:03:21			-85.66516667	167	107	
6:09:17	04:03:26	0	30.45765667	-86,6645	168	1,05	884
6:09:22	04:03:31	Q	30.45533333	-86.664	169	104	876
	04:03:36	Q	30.453	-86.6635	170	103	876
			30.45066667	-86.663	171	101	876
	04:03:41			and the second second			
6:09:37	04:03:46	0	30.44833333	-86.6626667	172	100	880
6:09:42	04:03:51	0	30.446	-86,66233333	174	99	884
60047	04:03:56	Ö	30,44366667	-86.862	174	100	572
				-86,66183333	175	102	860
	04:04:01						
	04:04:06	Ō	30.439	-86,6615	175	103	848
6:10:02	04:04:11	Ü	30.4365	-86.66123333	176	104	844
6:10:07	04:04:16	Ď	30,43416667	-86.66116667	177	104	840
	04:04:21			-86.66116667	178	105	852
						105	852
	04:04:26		30.42916667	-86.661	179		
6:10:22	04:04:31	G	30.42683333	-8 6.661	179	105	860
.6:10:27	04:04:36	0	30,42483333	-85,661	179	104	680
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				-86.66083333	178	103	928
	04:04:46	0					
	04:04:51			-86.66066667	179	102	952
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6:10:52 04:05:01	0 30,4125	-88,66066667	181	99	1012
6:10:57 04:05:06		-88.66056667	181	98	1044
		-86.65053333	181	97	1064
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6:11:27 04:05:36		-86,66116667	200	96	900
			227	96	844
6:11:32 04:05:41	0 30.39483333	-86.6625	· · · · · · · · · · · · · · · · · · ·	97	772
6;11:37 04:05:46		-86,66463333	250	Y .	720
6:11:42 04:05:51	0 30,39386667	-86.6675	271	100	
6:11:47 04:05:56	0 30.39386667	-85.67016667	273	102	712
6:11:52 04:06:01	0.30,39383333	-86.67283333	275	100	724
6:11:57 04:06:05	0 30.394	-86.6755	278	95	732
		-86.67763333	298	82	744
6:12:02 04:06:11				70	744
6:12:07 04:06:16	0 30.39586667	-86,6795	314		720
6:12:12 04:06:21	D 30.39663333	-86.68066667	325	63	
8:12:17 04:08:28	0 30.39816667	-86.6815	. 331	60	672
6:12:22 04:06:31	0 30:39983333	-88;68216667	337	58	632
6:12:27 04:06:35	0 30,40066657		342	58	612
			347	59	604
6:12:32 04:06:41	0 39.402	-86.68316667		56	584
6:12:37 04:06:46	0 30.40333333	-88,6835	351	•	
6:12:42 04:06:51	0 30,4045	-86.68366667	358	53	572
6:12:47 04:06:56	0.30.40566667	-86,68366567	357	50	556
8:12:52 04:07:01	0 30.407	-86.66366667	364	51	556
6:12:57 04:07:06	0 30,40816567		352	50	556
		-86.684	354	49:	552
6:13:02:04:07:11	0 30,40916667			49.	560
6:13:07 04:07:16	0 30,41033333		359	• "	564
6:13:12 04:07:2t		-86 564 15667	*	50	
6:13:17 04:07:26	0 30,41266867	-86.68416667	359	51	563
6:13:22: 04:07:31	0 30.414	-86.68416667	356.	40	564
6:13:27 04:07:36		-86.68433333	355	45	544
and the second s	0 30.416	and the second second	0	40	450
6:13:32 04:07:41			358	35	440
6:13:37 04:07:46	0 30,41683333			30	420
6:13:42 04:07:51	0 30,41766687	-86.6845	353		
6:13:47 04:07:56	0 30.41833333	-88.6845	254	27	380
6:13:52 04:05:01	0 30,419	-86.68466867	357	23	336
6:13:57, 04:08:06	0 30,4195	-86.68486667	350	25	300
	0 30.42016667	•	355	23	268
6:14:02 04:08:11		-86.68483333	354	21	220
6:14:07 04:08:16				22	192
8:14:12 04:08:21		-86.68483333	354		164
6:14:17 04:08:26	0 30,42166667	-96.58483333	356	:20	
6:14/22 04:08:31	0 30,422	-86,68483333	3 56	17	140
6:14:27 04:08:36	0 30,42203333	-86.685	357	14	116
6:14:32 D4:08:41	0 30,42266667	-86.665	357	5.5	104
	المصاحب المستحدث الم		356	8	88
6.14:37 04:08:46	0 30.42283333	-86.585		6	72
6:14:42 04:08:51	0 30,423	-88,685	37.5		48
6:14:47 04:08:56	0 30,42316667	-86,685	357	- 5	43
		0			
6:16:21 04:10:30	0 30,42333333	-86,685	355	1	58
		-86,685	350	13	76
6:16:26 D4:10:35			359	31	92
6:16:31 04:10:40	0 30,424	-86,665		48	124
6:18:36 04:10:45	0 30.42483333	-86,68516867	353		
8-18:41 04:10:50	0 30,42616667	-88.68533333	953	52	164
5:15:46 ()4:10:55	0 30.42783333	-86.6855	354	73	204
6:16:51 04:11:00		-86.68556657	354	82	248
	* ':	-86.68583333	356	89	292
6:16:50 D4:11:05		· · · · · · · · · · · · · · · · · · ·	300 356	\$3	340
6:17:01 04:11:10	0 30.4336 06 7	-86.586			380
5:17:0\$ 04:11:15		-86.66616667	359	97	
8:17:11 04:11:20	0 20:43816657	-88.68516887	1	99	428
6:17:16 04:11:25		-88.68566667	18	100	464
	0 30.4425	-86,6645	**	100	402
6,17:21 04:11:30		-85.68233333	83.	101	520
6:17:26 04:11:35			· · · · · · · · · · · · · · · · · · ·	102	552
6:17:31 04:11:40	0 30.44466657	-86.57983333	82		55 6
6:17:36 04:11:45		-86.67816667	85	104	
6:17:41 04:11:50		-88.67418657	\$5	105	552
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84746	04:11:55	0	30.44533333	-86,6715	84	104	592
	04:12:00	Õ		-66.60866667	83	102	632
			30.44583333	-86.666	84	97	692
	04:12:05	0				96	736
••	04:12:10	Q		-86,66333333	90		
6:18:06	04:12:15	Ũ	30.44566667	-86.66083333	103	95	772
6:18:11	04:12:20	0	30.445	-86.6 58 5	116	96	804
8-18-18	04:12:25	0	30.44366667		131	94	848
	04:12:30		30,44216667		145	96	884
				-86.6533 33 33	157	97	908
	04:12:35	0				100	924
	04:12.40	Ū	30.438	-86.6625	165		
6:18:36	04:12:45	O	30.43566657	-86.65183333	171	104	920
6:38:41	04:12:50	0	30.43316687	-86.6515	174	107	920
6:18:46	04:12:55	ü	30.43066667	-86:65133333	177	111	908
	04:13:00	ø		-86.65116667	179	115	880
A			30.425333333	* *	182	117	856
	04:13:05					112	858
	04:13:10	0	30.42266667		180		
0.19:06	04:13:15	O	30.42	-86.65116867	180	108	844
6:19:11	04:13:20	0	30.4175	-86.65116867	181	105	824
6:19:16	04.13:25	0	30.41516667	-86.65116667	180	103	806
	04:13:30	õ	30.41283333		180	1021	792
				-86.65133333	180	101	776
	04:13:35	0					776
	04:13:40	Ö		-86,65133333	179	101	
6:19:36	04:13:45	a	30.40566657	-86.65116667	175	101	776
6:19:41	04:13:50	0	30.40333333	-86.65116667	179	101	780
R-10-ZR	04:13:55	0	30.401	-86.65116667	180	102°	768
	04:14:00	õ	30.39866667		184	100	772
			.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		202	94	804
	04:14:05	0	30.396333333			92	804
	04:14:10	Q	30.3945	-86.653	225		
	04:14:15	0	30,3935	-86.65516667	252	83	784
6:20:11	04:14:20	Ü	30,39316657	-86.55766667	271	96	732
	04:14:25	0	30 39333333	-86.56016667	278	98	692
	04:14:30	Ű		-86.66283333	280	96	648
	04:14:35	g		-86.66533333	282	93	620
					282	82	596
	04:14:40	0		-86.66783333			
6:20:36	04:14:45	0		-86.67016667	284	92	576
6:20:41	04:14:50	Ö	30.39566667	-88.6725	289	90	572
6:20:46	04:14:55	0	30.39633333	-86.67483333	292	90	576
5/20/51	04:15:00	0	30 39716667	-86.677	297	87	580
	04:15:05	Õ	30.39816667	-86.679	302	88	584
					317	83	50 0
	04:15:10	0		-86,66083333		· ·	612
8:21:06	04:15:15	Ð		-86.68216667	332	79	
6:21:11	04:15:20	Q	30.40266667	-86.68283333	343	73	636
6:21:16	04:15:25	0	30.40433333	-86.68333333	351	76	632
	04:15:30		30,40616667	.86 R836667	355	76	592
	04:15:35	Ö		86.68365667	356	76	544
						74	508
	04:15:40		30.40966667		357		
6:21:36	04:15:45	0	30.41133333	-86.684	357	71	476
6,21:41	04:15:50	Ō	30.41283333	-86.684	357	64	452
	04:15:55	0	36.41433333	-86.68416667	356	56	424
	04:15:00	Ō		-86.68433333	354	47	408
				-86.68433333	355	41	372
	04:16:05	D		-,			
	D4:16:10	D	30.4175	-86.6845	356	37	336
6:22:06	04:16:15	0	30,41833333	-86.6845	358	34	304
6:22:11	04:16:20	0	30,419	-86.6845.	358	31	272
	04:10:25	0		-86,68466667	354	28	236
	04:16:30	Ď		-86.68466667	354	25	216
					353	23	192
	04:16:35	Õ		-86.68463333		20	160
	04:16:40	D.		-86.68483333	365		
6:22:36	04:16:45	O	30.42183333	-86.68483333	355	18	132
6:22:41	04:16:50	0	30.42216667	-86.685	354	14	112
	04:16:55	Ö	30.4225	-86.685	353	12	100
	04:17:00		30.42283333	-86,685	353	10	92
		Q					80
	04:17:05	0	30.423	-85,685	353	8	
6:23:01	04:17:10	O	30,42316667	-86.685	355	5	68
6:23:06	04:17:15	0	30.42333333	-86.685	351	3	48
	04:17:20		30.42333333	-85.685	350	1	32
Subdengage & S.	e.s Neg 245		- do so the second and any of the	Manager - Microsoft (No.			

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6:24:17	04:18:26	0	30,42333333	-86,685	350	2	60
	04:18:31	ŋ	30.4235	-86,685	350	14	80
6:24:27	04:18:36	û	30.424	-86,685	356	30	104
	04:18:41	Û		-86.68516667	354	49	128 180
	04:18:46			-86,88533333	350.	56 81	188 188
	04:18:51	û		-88.89566667	351	92 92	160 208
	04:18:56	0	30,43	-86.086	354.	## \$9	246
	04:19:01	Ü		-36.58633333	355 366	105	292
	04:19:06	0	30.4345	-86.8865	\$. 304	105	352
	04:19:11	Ü	30.437	-85.8565	25	102	#20
	04:19:16	Û	30.43933333	-86.66583333 -86.6 841 6667	49	99	408
	04:19:21			-86.68183333	73	150-	532
	04:19:26 04:19:31	ű		-80.57916667	23	163	588
	04:19:36	g g	30,443	-86.8769	86.	105	510
	04:19:41		30.44316667		87	106	660
	04:19:46.			-86.67083333	89	101	752
	04:19:51	O O	30,44316667	-88.86816867	100	96	848
	.04:19:58		30,4425	-88.68568667	115	94	916
	04:20:01	ά		-86,86366667	131	93	803
	04:20:05		The second second	-86,682	150	63	1060
	04:20:11	õ		-88,86116667	168,	Q4.	1096
	04:20:16	ā		-85.66083333	182	96	1112
	04:20:21	Ø	30.43316667	-86.867	184	96.	1104
	04:20:26	0	30.431	-86.66116867	184.	64 :	1112
6:26:22	04:20:31	Ò		-86.66133333	154	91	1096
8:26:27	04:20:36	0	30.42866667	-86.6615	164	9	1084 1044
	04:20:41	Q		-86.66183333	185	90	1008
	04:20:46	0	30.4225	-86.662	164	\$* \$*	972
	04:20:51	Ö		-83.66216867	*63 *82	92:	948
54 1 44	04:20:56		30.41833333	-98.88218867	*64 *81	93	936
	04:21:01	Ø.		-86.66233333	181	95	932
	04:21:05	Ö:		-86.66233333 -86.66233333	180	93	917
	04/21/11	Q 0		-86,66233333	180	<u>ē</u> 7	908
	04:21:16	9 å		-86.66233333	180	98-	896
	04:21:21 04:21:26	Ű		-86.66233333	180	100	878
	04:21:31	0		-86.86233333	178	tQ3-	860
	04:21:35	ă		-85,68218667	. 179	104	364
	04:21:41			-88.66216867	178	102	888
	04:21:46	õ	30.39533333	~86.662	177	102	900
	04:21:51	ā		-86.66183333	1.77	100.	904
	04:21:5%	á		-86,86166667	178.	97	928
6:27:52	04:22:01	0		-86.66166867	179	93.	948
6:27:57	04:22:06	Q.	30.38633333	-86.66166667	181	91	955
	04:22:11		30.38416667		102	91	952 944
	04:22:16	a		-86,66183333	162	90 69	940
	04:22:21	Q.	30.38	-86.662	182: 184	60 60	928
	04:22:26	0	30.37783333	-08.662	*0** 165	90 90	908
	04/22:31			-86.86218667	166	90	896
	04:22:36		30.37366667	-86.6625 na senacean	186	91	872
	04:22:41		30.37166667	-00.00200007 -86.663	186	91.	860
	04:22:46	Ģ	30.3595 30.36 7333 33		188.	90	0.08
	04:22:51				195	80.	889
	04,22:56		30.36533333	-86.66616667	207	90	868
	04:23:01		30.36166667		221	92	868
	04:23:06 04:23:11		30.36016867		236	03	872
	04:23:16		30.35916667	-86.67	251	94	872
	04:23:21		30:35886687		263	95	672
	04:23:28		30.35866667	-88.675	270	96	858
	04:23:31	õ		-86.67733533	304	95	856
	04:23:36	ã	30.361	-86.679	331	95	840
	04:23:41	0	30.38316667	-86.68	349	97	\$ 16
	04:23:46		10.36533333	-86.68033333	355	\$n	304

8:29:42	04:23:51	Õ	30.36766667	- 86 .6805	357	102	792
6:29:47	04:23:56	0	30.37016667	-86.88066667	¢	103	760
6:29:52	04:24:01	Ø	30.3725	-86.8805	٥	103	724
	04:24:06	0	30.375	-86.68066667	359	102	688
	04:24:11			-86.68066667	356	101	652
	04:24:16	*		-85.68083333	355	100	624
		ű			The state of the s		592
	04:24:21	0		-86.6811 6 567	356	100	
6:30:17	04:24:26	Û	30,384,33333	-86.68133333	357	100	548
6:30:22	04:24:31	Q.	30.38666667	-86,8815	358	tüt	476
6:30:27	04:24:36	0	30.389	-86.6815	358	101	408
	04:24:41	0	30.39133333	-86.68166667	358	100	348
	04:24:46	ő		-86.58183333	355	99	292
	04:24:51	Ö	,	-86.58216667	352	97	264
						94	252
	04:24:56	0	30.39816667	-86.6825	351		
	04:25:01			-86.68283333	354	91	256
6:30:57	04:25:06		30.40233333	-86.683	353	89	260
6:31:02	04:25:11	Q	30.40433333	-86.68333333	355	86	260
8:31:07	04:25:16	Ö	30.40633333	-86,6835	354	82	252
	04:25:21	Ö		-86.68366667	355	77	248
	04:25:26	Ö		-86.68383333	355	74	240
			30,41166667	-86.684	355	72	224
	04:25:31						192
	04/25:36			-86.68416667	355	68	
	04:25:41			-86.88433333	357	63	180
6:31:37	04:25:46	0	30.41616667	-86.6845	355	56	188
6:31:42	. 04:25:51	0	30,4175	-86.68466667	356	47	176
6:31:47	04:25:56	0	30,4185	-86.68466667	356	43	156
6:31:52	04:26:01	Ö	30.4195	-86.68466667	356	40	128
	04:26:06			-86.68483333	356	37	108
	04:26:11	ő		-86.68483333	357	37	72
				-86.685	356	21	58
6/3///07	04:26:16	0	30.422		439A,	Ζ. !	يهاد.
				0	***	_	m/h
	04:36:34	0		-86.68516667	342	3.	56
6:42:30	04:36:39	٥		-86.58516667	347	18	84
6:42:35	04:36:44	0	30.42566567	-86.68533333	350	39	116
6:42:40	04:36:49	0	30.42666667	-86.68556667	347	58	144
R-47-45	04:36:54	٥	30,42833333	-86:686	347	74	176
.,,	04:36:59	ő	30.43	-86.6865	349	85	212
	04:37:04	ŏ		-86.68683333	354	91	256
			30.43433333	-86.687	357	96	284
	04:37:09	0					308
	04:37:14	0	30.4365	-86.687	359	. 99	
6:43:10	04;37:19	0	30.43883333	-86.687	4	101.	316
8:43:15	04:37:24	. 0		-86.68666667	10	100	336
6:43:20	04:37:29	Ğ	30.4435	-86.68616667	15	99	364
6:43:25	04:37:34	Ø-	30.44566667	-86,68533333	21	100	388
	04:37:39	à	30.44783333	-86 684 16667	30	100	388
	04:37:44	ũ		-86.68266667	38	100	368
	04:37:49		30.4515	-86.681	40	98	344
		a				96	340
	04:37:54	0		-86.67933333	41		
	04:37:59	ů,	30.455	-86.6775	41	98	328
	04:38:04	0		-86.67583333	41	99 -	308
6:44:00	04:38:09	0	30.45833333	×86.674	41	100	304
6:44:05	04:38:14	Ó	30,46016667	-86.67233333	41	99	380
8:44:10	04:38:19	Ü	30.46183333	-86.5705	41	99	488
	04:38:24	ä	30.46366667	-86.66866667	41	102	544
	04:38:29	ŏ		-86.66683333	42	105	589
					42	108	576
	04:38:34	0	30.46733333	-86.665			560
	04:38:39	O	30,46916667	-86,663	42	110	
6:44:35	04:38:44	0	30.47116687	-86.861	40	112	504
6:44:40	04.33:49	Û		-86.65916667	40	111	466
8:44:45	04:38:54	0		-86.65716667	. 41	107	456
	04:36:59	ő		-86.65533333	41	106	436
	04:39:04	å	30,47883333	-86.6535	39	105	428
	04:39:09		30.48066667		39	107	392
					37	107	352
	04:39:14	0	30.48266687	-86.65		106	348
	04:39:19		30.48466667		36		
6:45:15	04:39:24	Q	30.48666667	-25.6465	36	106	324

8:45:20 04:39:29	0 30,488666	7 -86.64456667	38		304
6:45:25 04:39:34	G 30.450	586:043	40	103	300
6:45:30 04:39:39	0 30,4923333	3 -88.64118667	41	103	296
6:45:35 04:39:44		7 -86,63933333	41	103,	292
6:45:40 04:39:49	0 30,49	6 -86,6375	40	102	296
6:45:45 04:39:54	0 30.4978333	"	39	102	304
6:45:50 04:39:59	0 30.4996886			102	308
The state of the s		6 - 6 6.6323333	šγ	103	292
6:45:55 04:40:04			j?	105	288
6,46,00,04,40:09				108	280
8:46:05 04:40:14	Ü 30.505		32 32	105	292
6:46:10 04:40:19	0 30,507		28	105	316
6:46:15 04:40:24	0 30 5096666			105	324
6;46;20 04;40;29		3 -86.62483333	23	105	328
6:46:25 04:40:34		7 -86.62383333	18	105	336
6:46:30 04:40:39		5 -50.82316667	11		352
6:46:35 04:40:44		3 -86.62266667	\$	103	
6:46:40 04:40:49	0 30 5213333		8.	102	364
6:45:45 04:40:54	0 30.5236666	7 -85.622	10	101	360
6:45:50 04:40:59	0 30.52	5 -88.6215		100	344
6:46:55 04:41:04	0 30,5281666	7 -86.621	10	97	340
8:47:00 04:41:09	0 30 5203333	3 -86.6205	10	95	344
8:47:05 04:41:14		5 -86.62016657	10	94	348
8:47:10 04:41:19	1	7 -86.61966657	10	93	352
5:47:15 04:41:24	0 30.5368333		10	9.2	352
	0 30.53			92	348
6;47:20 04:41:29	0 30.54		8	91	356
6:47:25 04:41:34		7 -36.61616667	8	90	372
8:47:30 04:41:39	W 100 00 00 00 00 00 00 00 00 00 00 00 00		8	89	372
6:47:35 04:41:44			ğ.	91	364
6:47:40 04:41:49	0 30.6473333		19	93	356
6:47:45 04:41:54	0 30.549		** 8	93	360
6:47:50 04:41:59		7 -88,61668667	7	Ğ4	388
6:47:55 04:42:04	0 30.5538333		"	8	364
6:48:00 04:42:09	0 30.55			96	364
8:48:05 04:42:14		7 -86,61560667	8:	97	352
6:48:10 04:42:19	0 30.5603333				328
6:48:15 04:42:24		7 -86,61463333	10	100	304
6:46:20 04:42:29	0 30.56		11	102	
6:48:25 04:42:34	0 30,5673333	3 -85.61383333		103	292
6:48:30 04:42:39	0 30.5696668	7 -88:61315667	12	104	300
6:48:35 04:42:44	0 30.57	2 -86.61285667	11	104	310
6:48:40 04:42:49	0 30,574	5 86,51216667	11	104	316
6:48:45 04:42:54	0 30,5768333	3 -86,61166667	11	104	328
6:48:50 04:42:59	0 30.5791666	7 -86.611	10	104	324
6:48:55 C4:43:C4		7 -88.61068667	Q.t.	103	332
6.49.00 04.43.09	0 30.59	***	10	.102	340
6:49:05 04:43:14	0 30.5883333	and the second second	10	103	340
6:49:10 04:43:19	0 30.5886666	7 -86.60916567		103	344
6:49:15 04:43:24	g 30.59		د. د. د. د	102	338
6:49:20 04:43:29	0 30.5933333		and the second s	101	352
	0 30.5956666			101	348
6:49:25 04:43:34			11	102	236
6:49:30 04:43:39		3 -86 60 6 33333		102	340
6:49:25 04:43:44		a -00.000000000 - Ad-Abeanni		102	340
6;49:40 04:43:49		5 -86.60583333	11	102	348
6:49:45 04:43:54		3 -86.60533333		102	344
6,49:50 (4:43:59		7 -86.60483333	11	101	336
6:49:55 04:44:04		5 -86.60433333	1.1	101	336
6.50:00 04:44:09	0 30.6118333	3 -86.60383333	10	and the second s	336
6:50:05 G4:44:14	0 30.6141656	7 -85.60333333	10	100	
6:50:10 D4:44:19		ā -86.60283333		98	340
6:50:15 04:44:24	0 30,618666	7 -85.60233333	10	97	356
6:50:20 04:44:29	0 30.63	1 -86:602	9	96	352
6:50:25 04:44:34		7 -86,80168667	9	96	340
6.50:30 04:44:39		3 -86,60116667	9	94	352
6:50:35 04:44:44		5 -86.60083333	10	91	368
6:50:40 04:44:49		5 -86.60033333		90	376
8.50.45 04.44.54	0 30 63 1966			.91	368
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6:50:50	04:44:59	0	30.53366667	-86.5095	10	91	364
6:50:55	04:45:04	0	30.63583333	-86.59918567	11	91	364
6:51:00	04:45:09	O	30.63783333	- 86.598 66667	11	91	380
6:51:05	04:45:14	D	30.64	-86.59816667	* **	93	400
6:51:10	04:45:19	Ü	30,64216667	-86.59766667	11	95	412
6:51:15	04:45:24	0	30.64433333	-86.59716067	10	96	424
6:51:20	04:45:29	٥	30.6465	-86,59666667	9	86	404
6:51:25	04:45:34	0	30.64883333	-86.5963333 3	8	99	376
6:51:30	04:45:39	0	30.651	-86.59583333	9	98	364
6:51:35	04:45:44	Û	30.65333333	-8 ö.5955	8	98	360
6:51:40	04:45:49	0	30,65566667	-86,59566637	344	98	396
6:51:45	04:45:54	Ü	30.65766667	-86.59683333	317	100	412
6:51:50	04:45:59	0	30.659	-86.599	296	101	412
6:51:65	04:46:04	0	30-65983333	-86,60166667	288	103	388
6:52:00	04:46:09	0	30,6805	86.60433333	287	104	376
6:52:05	04:46:14	0	30.66116667	-86.607	285	106	372
6:52:10	04:45:19	٥	30.66183333	-86.60983333	283	109	372
6:52:15	04:46:24	0	30.66233333	-86.61266667	282	110	372
6:52:20	04:46:29	0	30 66283333	-86.61566667	262	112	372
6:52:25	04:46:34	Q.	30 66333333	-86.6185	285	1.11	364
6:52:30	04:46:39	Q	30.6645	-86.62116667	306	106	364
6:52:35	04:46:44	Q	30.66633333	-86.623	335	101	360
6:52:40	04:46:49	O .	30.6685	-86.62366667	359	100	332
6:52:45	04:46:54	0	30.67083333	-86.62316667	22	98	312
6:52:50	04:46:59	0	30.67266667	-86.62166667	46	98	312
6:52:55	04:47:04	0	30.674	-86.6195	70	99	328
6:53:00.	04:47:09	0	30,87433333	-86.61683333	:90	100	340
6:53:05	04:47:14	0	30.67433333	-86.61416667	90	100	324
6:53:10	04:47:19	0	30.67433333	-86,6115	90	99	308
6:53:15	04:47:24	0	30.67433333	-86,60883333	89	99	308
6:53:20	04:47:29	٥	30.67433333	-86,60633333	90	93	312
6:53:25	04:47:34	0	30.67433333	-86,603 63333	90	83	316
6:53:30	04:47:39	Ü	30.67433333	-86,60183333	91	73	320
8:53:35	04:47:44	Ö	30.67433333	-8 6.6	92	66	340
6:53:40	04:47:49	O	30,67416667	-86,59833333	94	58	360
6:53:45	04:47:54	Q	30.674	86,59683333	96	54	368
6.53.50	04:47:59	Ü	30.674	-86.59533333	95	51	388
6:53:55	04:48:04	0	30.67383333	-86.594	87	49	358
6:54:00	04:48:09	0	30.674	-86,59283333	. 80	40	328
6:54:05	04:48:14	0	30.67416667	-86.59183333	72	29	300
6:54:10	04:48:19	Ø	30.67433333	-86.59133333	79	19	284
6:54:15	04:48:24	0	30.67433333	-86.59083333	89	9	264
6:54:20	04:48:29	0	30.67433333		90	4	256
6:54:25	04:48:34	Q	30.67433333	-86,59033333	97	24	256
	04:48:39	0	30.87416567	-96.5395	122	.41	256
- ; •	04:48:44	0		-86.588 833 333	164	47	256
	04:48:49	0	30.67233333	-86.589	228	45	244
	04:48:54	Û	30.67216667	-86.59	288	36	244
	04:48:59	Õ	30:6725	-86.59066667	329	26	240
	04:49:04	Ö	30.673	-86,591	337	20	236
	04:49:09	Ö		-86.59116667	340	16	218
	04:49:14	ő	30.67383333	-86.59133333	353	14	196
	04:49:19	ű		-86.59133333	191		112
wenter and the state	- 7 5 mws - 4 M	200	- North Color of A	- women's a bank many			

	TIME		Lat System degrees	Long_System degrees	Groundtrack_System degrees	Groundspeed_System knots		THOG_Sys degrees
	04/49/20		-			•		
8:55:15	04:49:24	Ö	30.674	-86.59133333	334	ំព	108	
6:55:20	04:49:29	Ö	30.674	-86.59135333	330	Ü	112	
	04:49:32		30.674038	-86:591308	333.4	0.13	112	333.4

Pitch_Sys Roll_Sys VN_Sys VE_Sys VV_Sys VN_GPS VE_GPS VV_GPS Attitude_GPS Lat_GPS Long_GPS Attitude_INS degrees degrees feet

Pitch_Sys Roll_Sys VN_Sys VE_Sys VV_Sys VN_GPS V5_CPS VV_GPS Altitude_GPS Lat_CPS: Long_GPS Altitude_tNS degrees degrees feet degrees degrees feet degrees degrees feet 3.31 10.1 -9.484 100 30.673997 -88.5913215

0.235 -10.5 0.068 -0.202 0.504

112

Lat INS Long INS VN INS VE_INS VV INS AN INS AE INS AZ INS Pitch INS Roll INS Pitch Rate INS Roll Rate INS degrees degrees degrees degrees degrees degrees degrees.

Lat_INS Long_INS VN_INS VE_INS VV_INS AN_INS AE_INS AZ_INS Plich_INS Roll_INS Plicb_Rate_INS Roll_Rate_INS degrees deg

THDG_INS_MHDG_INS_Turn_Rate_Sys_HDG_Ref_Sys_Attitude_Ref_Sys_Navigation_Mode_INS_Figure_of_merit_CDU_Screen degrees degrees degrees degrees.

THOG INS MHDG INS Turn_Rate_Sys HDG_Ref_Sys Attitude_Ref_Sys Navigation_Mode INS_Figure_of_merit_CDU_Sgreen degrees degrees degrees degrees

333.4

334.3

0.0712 Magnetic

INS

Kalman-inertial

9 Present_Position

Pilot_HDD_Display Pitot_HDD_Declutter Copilot_HDD_Display Copilot_HDD_Declutter Map_Mode Map_Scale

Pilot_HDD_Display Pilot_HDD_Declutter Copilot_HDD_Display Copilot_HDD_Declutter Map_Mode Map_Scale

Hover Mode_A Hover Mode_A Imagery 1_NM